

Sc³⁺-modified Mg–Al–Mn–Fe–O spinel ceramics with co-enhanced microwave dielectric and thermosensitive properties for multifunctional applications

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ABSTRACT: With the rapid development of communication technology, multifunctional ceramics that integrate microwave dielectric and negative temperature coefficient (NTC) thermistor properties have met the evolving needs of electronic components. Although conventional spinel oxides excel in single functionalities, they struggle to simultaneously achieve linear NTC behavior and stable microwave dielectric performance over a wide temperature range. To address this, the role of Sc³⁺ substitution in modifying Mg_{0.8}Mn_{0.2}Al_{1.6}Fe_{0.4}O₄ ceramics was systematically investigated. The results demonstrate that Sc³⁺ substitution effectively inhibits oxygen vacancy formation and achieves the ratio regulation of the Mn²⁺/Mn³⁺ and Fe³⁺/Fe²⁺ bimetallic redox pairs, which significantly improves the material constant B ($B_{200/1000^\circ\text{C}} = 8367\text{--}9758\text{ K}$) and enables linear resistance–temperature curves ($\ln R\text{--}1000/T$) within a broad temperature range (200–1000 °C). Additionally, the ceramics exhibit optimal microwave dielectric properties: low dielectric constants ($\epsilon_r = 8.86\text{--}10.55$), ultrahigh quality factors ($Q\text{--}f = 96,000\text{--}149,000\text{ GHz}$), and near-zero temperature coefficients of resonant frequency ($\tau_f = -33.2 \times 10^{-6}$ to $-10.2 \times 10^{-6} \text{ }^\circ\text{C}^{-1}$), resulting from Sc³⁺-induced lattice stabilization and octahedral bond-valence strengthening effects. A cylindrical dielectric resonator antenna (CDRA) fabricated from Mg_{0.8}Mn_{0.2}Al_{1.3}Sc_{0.3}Fe_{0.4}O₄ achieves 92% radiation efficiency and 6.28 dBi gain at 12 GHz, validating its potential for Ku-band satellite communication. This work reveals that Sc³⁺ substitution synergistically enhances both the microwave dielectric and thermosensitive functionalities of Mg–Al–Mn–Fe–O spinel ceramics, offering a breakthrough in material design for next-generation multifunctional communication devices.

KEYWORDS: microwave dielectric properties; negative temperature coefficient; spinel; multifunctional ceramics

1 Introduction

The rapid advancement of communication technology has become a cornerstone for promoting the development of the digital economy [1–3]. As the technological paradigm has evolved from the internet of everything (IoE) to the space–air–ground–sea-integrated network (SAGSIN), multifunctional ceramics have emerged as pivotal dielectric materials to overcome critical bottlenecks in next-generation communication systems through synergistic integration of material properties and technological innovations. Although significant progress has been made in the development of multifunctional ceramics, including magnetic–microwave dielectric [4,5], ferroelectric–luminescent [6,7], magnetic–thermosensitive [8], and piezoelectric–transparent [9,10] ceramics, the integration of microwave dielectric and

negative temperature coefficient (NTC) thermosensitive functionalities remains an uncharted territory. Microwave dielectric ceramics have garnered substantial research interest in microwave communication applications (shown in Fig. S1 in the Electronic Supplementary Material (ESM)), primarily owing to three key characteristics: 1) tunable dielectric constants (ϵ_r) that satisfy device miniaturization requirements, 2) high $Q\text{--}f$ values (where $Q = 1/\tan\delta$, and f represents the resonant frequency) enabling enhanced frequency selectivity, and 3) near-zero temperature coefficients of resonant frequency (τ_f) ensuring thermal stability [11,12]. Simultaneously, NTC thermistors have established themselves as indispensable “thermal managers” in communication systems, offering high precision, rapid response, broad operational temperature ranges, and cost effectiveness. Given these properties, the development of

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microwave dielectric-thermosensitive multifunctional ceramics has significant potential.

Spinel oxides (AB_2O_4) have become a focal point in the field of materials research because of their multifunctional properties for optical, electrical, magnetic, and catalytic applications [13–16]. Recent studies have extended their applications to microwave dielectrics because of their inherent low dielectric constant ($\epsilon_r < 10$) and small loss tangent ($\tan\delta < 0.001$), which are essential for high-frequency communication systems. Within this family, $MgAl_2O_4$, which has a cubic spinel structure, is the most representative. Shannon *et al.* [17] first reported the dielectric properties of $MgAl_2O_4$ single-crystal ceramics measured at 1 MHz in 1991, with $\epsilon_r = 8.325$ and $\tan\delta = 0.0008$. By 2005, Sebastian and colleagues succeeded in obtaining $MgAl_2O_4$ ceramics with excellent microwave dielectric properties ($\epsilon_r = 8.8$, $Qf = 68,900$ GHz, and $\tau_f = -75 \times 10^{-6} \text{ }^\circ\text{C}^{-1}$) [18], which surpassed their previously reported $ZnAl_2O_4$ ceramic ($\epsilon_r = 8.5$, $Qf = 56,300$ GHz, and $\tau_f = -79 \times 10^{-6} \text{ }^\circ\text{C}^{-1}$) [19]. Notably, owing to its high-temperature stability and ultrawide bandgap, $MgAl_2O_4$ is expected to serve as a high-temperature thermistor following ion doping or composite engineering [20,21]. Through such strategies, the inherent dielectric properties can synergize with the thermal sensitivity, enabling the realization of microwave dielectric-thermosensitive multifunctional ceramics.

Previous studies have shown that achieving complete densification through composite modification is difficult [22]. Therefore, solid solution modulation is an excellent strategy for achieving property integration while maintaining structural integrity [23]. $MnFe_2O_4$ shares the same $Fd\bar{3}m$ space group as $MgAl_2O_4$ and generally has an inverse-spinel or semi-inverse-spinel structure [24]. Studies have further demonstrated that $MnFe_2O_4$ has low ϵ_r and $\tan\delta$ values, suggesting its potential for use in microwave dielectric applications [25]. Moreover, the valence transitions of Mn/Fe ions under external stimuli result in the formation of mixed valence states of Mn^{2+}/Mn^{3+} and Fe^{2+}/Fe^{3+} , implying their suitability as NTC thermistor materials due to their enhanced electrical conductivity. On the basis of the small polaron hopping model, the conductivity can be attributed to electron hopping between variable valence states of the cations [26]. However, $MgAl_2O_4$ is unsuitable for thermistors due to its high resistivity, while $MnFe_2O_4$ suffers from poor stability and low resistivity, precluding high-temperature applications. Hence, our previous work [8] took advantage of this structural consistency to prepare $Mg_{1-x}Mn_xAl_{2-x}Fe_{2(1-x)}O_4$ ceramics by solid solution modulation. When $x = 0.8$, the $Mg_{0.8}Mn_{0.2}Al_{1.6}Fe_{0.4}O_4$ ceramic has a high B ($B_{100/1100^\circ\text{C}} = 8056$ K) value and the lowest aging coefficient, which is expected to provide accurate temperature measurements over a wide temperature range and in the high-temperature region. However, non-Arrhenius behavior persists in the electrical properties above $700 \text{ }^\circ\text{C}$ (coefficient of determination for $\ln\rho$ and $1000/T$ (R^2) < 0.98), resulting from charge equilibrium disruption induced by B-site metastable ion migration. This phenomenon occurs when variable-valence ions are present in the spinel structure [27,28] and represents a key challenge requiring resolution.

The 4f-electron configuration of rare-earth elements dictates their unique atomic structures and physicochemical characteristics, endowing them with distinctive optical, electrical, magnetic, and thermal attributes. As a result, rare-earth ion modifications play critical roles in microstructure evolution, lattice stabilization, and dielectric behavior. Although the more commonly used rare-earth elements are Nd, Y, Sm, Ce, and Sc have important roles in stabilizing the crystal structure of solid oxide electrolytes and modulating ion mobility [29,30]. Building upon this rationale, we designed a series of $Mg_{0.8}Mn_{0.2}Al_{1.6-x}Sc_xFe_{0.4}O_4$ ($x = 0-0.4$, denoted $y\text{Sc-MMAFO}$ where $y = 10x$) via B-

site substitution, with $Mg_{0.8}Mn_{0.2}Al_{1.6}Fe_{0.4}O_4$ as the substrate. The crystal structures, microstructures, thermosensitive properties, and microwave dielectric properties of the ceramics were also fully characterized and analyzed. As expected, Sc^{3+} substitution effectively addressed the problem of poor linearity due to the variation in B values in the high-temperature range, and excellent microwave dielectric properties were also obtained. Importantly, the 3Sc-MMAFO ceramic was designed into cylindrical dielectric resonator antennas (CDRAs) via CST Microwave Studio 2019 simulation software, and prototype CDRAs were fabricated to realize Ku-band satellite communication applications. Ultimately, Sc^{3+} -modified Mg–Al–Mn–Fe–O spinel ceramics synergistically optimize the microwave dielectric and thermosensitive properties, which provide a pathway to advance multifunctional integration strategies for 6G communication front-end systems.

2 Experimental methods

Multifunctional $y\text{Sc-MMAFO}$ ($y = 1-4$) ceramics were synthesized via a conventional solid-state reaction method. The detailed synthesis procedures (shown in Fig. S2 in the ESM) were reported in our previous study [8]. In this study, the sintering temperature of the ceramics was $1510 \text{ }^\circ\text{C}$. The structures of the ceramics were characterized by an X-ray diffractometer (XRD; D8-Advance, Bruker, Germany) using $\text{Cu K}\alpha$ radiation in the 2θ range from 0° to 90° with a scanning speed of $0.2 \text{ }^\circ/\text{s}$. The Raman spectra were recorded at room temperature (RT) via a LabRAM HR Evolution confocal Raman microscope (Horiba, France). The phase information was analyzed via Rietveld refinement of the XRD patterns using GSAS-II software. The microstructure and composition of the sintered pellets were observed by a scanning electron microscope (SEM; SUPRA 55 VP, Zeiss, Germany) in combination with an energy dispersive spectrometer (EDS; Nano GmbH Berlin, Bruker, Germany). The grain size was measured using the intercept method, and the number of tested grains was greater than 100. A cross-section of a ceramic sample for electron microscopy was prepared by focused ion beam (FIB) thinning. High-resolution transmission electron microscopy (HRTEM) of the samples was performed via a transmission electron microscope (TEM; JEOL, JEM-2100F, Japan). The chemical state of the as-sintered pellets was determined via an X-ray photoelectron spectrometer (XPS; Thermo Scientific, Escalab 250Xi, USA) with $\text{Al K}\alpha$ radiation at RT. The XPS results of all elements were calibrated against the standard C 1s peak. The XPS data were analyzed through Gaussian–Lorentzian curve fitting, where the parameters were optimized such that the fitting function was closest to the actual energy spectrum curve. An electron paramagnetic resonance spectrometer (EPR; Bruker D300, Germany) was used to detect the presence of oxygen vacancies on the surface of the material.

To measure the electrical properties, the parallel faces of the sintered samples were coated with platinum paste and then annealed at $900 \text{ }^\circ\text{C}$ for 30 min. Direct-current (DC) resistance measurements were conducted from 200 to $1000 \text{ }^\circ\text{C}$ via a Fluke 2638A data acquisition system coupled with a Fluke 9150 furnace and Fluke 1586A multiplexer (USA). The material constant B and sensitivity coefficient (α_T) can be calculated via Eqs. (1) and (2):

$$B = \frac{\ln(\rho_1/\rho_2)}{1/T_1 - 1/T_2} \quad (1)$$

$$\alpha_T = -\frac{B}{T^2} \quad (2)$$

where ρ_1 and ρ_2 are the resistance values at the absolute temperatures of T_1 and T_2 , respectively, and T is the absolute temperature (in Kelvin). Impedance spectroscopy was measured

via an impedance analyzer (E4980AL, Keysight, USA) over a frequency range of 20 Hz–1.78 MHz and a temperature range of 25–1200 °C. The microwave dielectric properties (ϵ_r , Qf) were evaluated via the TE_{01δ} (TE_{01δ} refers to a specific electromagnetic resonance mode in dielectric resonators) resonant mode method with a vector network analyzer (E5063A, Keysight, USA). The resonance frequency was measured at various temperatures, and Eq. (3) was used to calculate τ_f of the ceramics:

$$\tau_f = \frac{f_{85} - f_{25}}{f_{25}(85 - 25)} \times 10^{-6} \quad (3)$$

where f_{85} and f_{25} correspond to the resonant frequencies measured at temperatures of 85 and 25 °C, respectively. CDRA was designed and simulated via CST Microwave Studio 2019 simulation software. To evaluate the performance of the antenna, the reflection parameters S_{11} were measured via a microwave network analyzer. The experimental procedures were outlined as follows: the ground plate material was the Rogers RT5880 substrate, characterized by $\epsilon_{r,sub} = 2.20$ and $\tan\delta = 0.0009$. Additionally, metallic copper was employed as the electrode material on the substrate, with electrode structures fabricated via printed circuit board technology. The CDRA was fabricated from Mg_{0.8}Mn_{0.2}Al_{1.3}Sc_{0.3}Fe_{0.4}O₄ ceramics through wire-cutting of simulation-optimized geometries, and subsequently bonded to the center of the metal ground plate by conductive epoxy.

3 Results and discussion

3.1 Design of Mg_{0.8}Mn_{0.2}Al_{1.6}Fe_{0.4}O₄-based multifunctional ceramics

3.1.1 Crystal structure analysis

Figure 1(a) shows the XRD patterns of the γ Sc-MMAFO

ceramics. The main phase corresponds to the spinel structure of MgAl₂O₄ in the $Fd\bar{3}m$ space group. A Sc₂O₃ secondary phase (PDF#05-0629) emerges at $x \geq 0.02$, attributed to the limited solubility of Sc³⁺ in the spinel lattice and complex sintering kinetics. To explore the internal structural features in detail, Rietveld refinement was performed on a representative 3Sc-MMAFO ceramic, as depicted in Fig. 1(b) (the results for the other samples are displayed in Fig. S3 and Table S1 in the ESM). The refined confidence coefficients (R_{wp}) are less than 10%, and the χ^2 values are small, confirming that the results are reliable. Figure 1(c) presents the crystallographic framework of the ceramic sample. This structure comprises a continuous network of tetrahedral and octahedral units that form the primary lattice. Variable valence ions can be located in both the A and B sites of the spinel, and Sc³⁺ can only occupy the octahedral B site. Therefore, its chemical formula can be written as [Mg_{0.8}Mn_{0.2-i}Fe_i]_{tetra}[Al_{1.6-x}Sc_xMn₁Fe_{0.4-i}]_{oct}O₄ (where i denotes the degree of spinel inversion). As shown in Fig. 1(d), the lattice parameters linearly expand with increasing Sc³⁺ concentration y ($a = b = c$: 8.082 → 8.117 Å; V : 527.8 → 535.1 Å³), following Vegard's law [31]. This monotonic expansion directly correlates with the larger ionic radius of Sc³⁺ (0.745 Å) than that of Al³⁺ (0.535 Å).

3.1.2 Raman spectral analysis

Compared with XRD, Raman spectroscopy is more sensitive to short-range structural distortions. The deconvoluted Raman spectrum in the range of 100–870 cm⁻¹ shown in Fig. 1(e) was fitted via a Gaussian–Lorentzian function, resolving five eigenmodes consistent with the group theory prediction for $Fd\bar{3}m$ spinel: $\Gamma_{\text{Raman}} = E_g + A_{1g} + 3T_{2g}$ (where the $3T_{2g}$ mode is labeled T_{2g}^1 , T_{2g}^2 , and T_{2g}^3 on the basis of wavenumber) [32,33]. High-frequency modes (> 650 cm⁻¹) originate from symmetric A/B–O stretching vibrations within octahedral [A/BO₆] units [34], whereas mid-range modes (300–650 cm⁻¹) arise from asymmetric

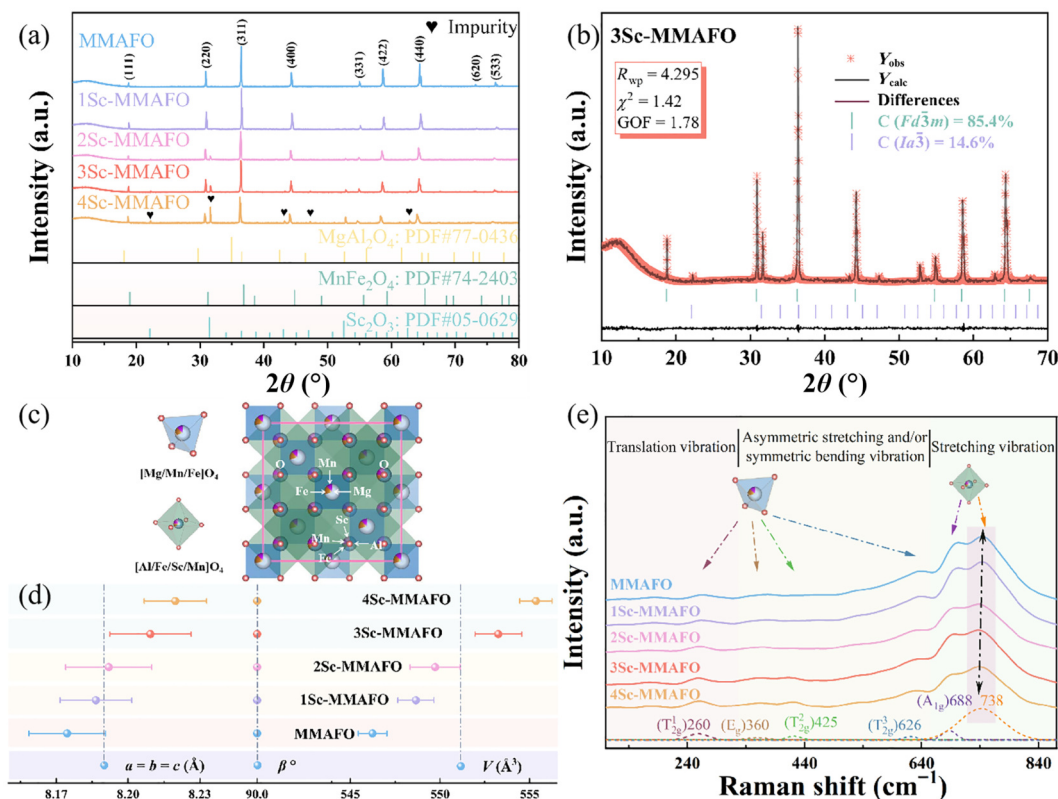


Fig. 1 Structural analysis of ceramics. (a) XRD; (b) Rietveld refinement XRD results for 3Sc-MMAFO ceramic; (c) schematic of crystal structure; (d) evolution of lattice constants as a function of y ; (e) Raman spectra.

stretching/bending in tetrahedral $[A/BO_4]$ sites [32,35]. Low-frequency modes ($< 300 \text{ cm}^{-1}$) are assigned to translational motions of tetrahedral units [36]. The broad asymmetric bands in the E_g and A_{1g} modes are typical of synthetic spinels [37]. Furthermore, the observed redshift of the A_{1g} mode (Fig. 1(e)) directly confirms lattice expansion. This phenomenon arises from the increased interatomic bond lengths induced by lattice expansion, which drives the crystal lattice into a more relaxed state, thereby reducing the vibrational frequency and ultimately attenuating the Coulombic interactions between cations and anions [32].

3.1.3 Density and microstructure analysis

The theoretical density (ρ_{theo}) was calculated via crystallographic parameters (Eq. (4)):

$$\rho_{\text{theo}} = \frac{Z \times A}{V_{\text{cell}} \times N_A} \quad (4)$$

where A , Z , N_A , and V_{cell} denote the molar mass, number of cells per molecule, Avogadro constant, and unit cell volume, respectively. The relative density (ρ_r) of the sample is the ratio of its bulk density ρ_{bulk} to ρ_{theo} and is given by Eq. (5):

$$\rho_r = \frac{\rho_{\text{bulk}}}{\rho_{\text{theo}}} \quad (5)$$

All samples exhibit high relative densities ($> 98\%$) (Fig. S4(f) in the ESM), implying that density, porosity, and grain size have negligible effects on the quality, which plays an important role in reducing $\tan\delta$ (enhancing the $Q \cdot f$ values). Furthermore, SEM images of the polished and thermally etched ceramic surfaces are shown in Figs. S4(a)–S4(e) in the ESM, revealing uniform grains, relatively well-defined grain boundaries, and a few visible pores. Residual porosity arises from oxygen evolution during solid-state synthesis, as evidenced by the redox reaction: $1.6\text{MgO} + (1.6-x)\text{Al}_2\text{O}_3 + 0.4\text{MnO}_2 + 0.4\text{Fe}_2\text{O}_3 + x\text{Sc}_2\text{O}_3 \rightarrow 2\text{Mg}_{0.8}\text{Mn}_{0.2}\text{Al}_{1.6-x}\text{Sc}_x\text{Fe}_{0.4}\text{O}_4 + 0.4\text{O}_2$. Sc^{3+} substitution induces significant grain refinement, with the average grain size decreasing from $12.86 \mu\text{m}$ ($y = 0$) to $2.47 \mu\text{m}$ ($y = 4$) (Figs. S4(a)–S4(e) in the ESM). The tunability of the grain size proves that Sc^{3+} is an effective microstructure modifier and provides a controllable substitution strategy for performance optimization.

A comprehensive microstructural characterization of the sample with $y = 3$ was conducted through correlated HRTEM and selected-area electron diffraction (SAED) analyses. As shown in Fig. 2(a), there is atomic-scale agreement between the refined XRD structural model projected along the axis of the $[211]$ region and the inverse fast Fourier transform (IFFT) image of the HRTEM region. Small amounts of the secondary phase Sc_2O_3 are present but have little effect on the structure. Notably, the IFFT-processed image in Fig. 2(c) shows contrast undulations, indicating the presence of localized lattice distortions in the ceramic matrix. The normal strains along the xx and yy directions were derived from geometric phase analysis (GPA) calculations, which revealed that compressive strains were accompanied by a small amount of symmetric tensile–compressive strains (Figs. 2(d) and 2(e)). The quantitative results (as shown in Fig. S5 in the ESM) indicate that the compressive strain is significantly greater than the tensile strain, which is related to the lattice expansion due to greater cation substitution. The HRTEM image (Fig. 2(f)) shows clear lattice fringes with a measured facet spacing of approximately $2.8 \text{ \AA}$, indexed to the (022) plane for the 3Sc-MMAFO ceramic. The absence of diffraction spot splitting in the SAED pattern of Fig. 2(g) further confirms the excellent crystallinity of the material. EDS elemental mapping (Fig. 2(i)) revealed a homogeneous distribution of Mg, Mn, Al, Sc, and Fe at submicron scales, confirming the chemical homogeneity of the solid solution.

3.1.4 XPS analysis

Figure 3 presents the XPS spectra of Fe 2p, Mn 2p, O 1s, and Sc 2p. Fitting the XPS spectra with a Gaussian–Lorentzian function revealed that the binding energies of Fe^{2+} , Fe^{3+} , Mn^{2+} , and Mn^{3+} are within the ranges of 710.11 – 710.58 , 711.78 – 712.54 , 640.43 – 640.92 , and 641.60 – 642.44 eV , respectively. In addition, the positions of the XPS peaks of all the characteristic elements shifted with increasing Sc^{3+} substitution. This is mainly due to the change in the binding energy required to form a stable lattice, which is also the second phase of Sc_2O_3 . Notably, as the degree of Sc^{3+} substitution increases, the Fe 2p, Mn 2p, and O 1s XPS peaks shift to the left at first and then gradually shift to the right, which means that Sc^{3+} substitution increases the binding energy when $y = 1$. This is because at this point, the lattice mismatch is at its

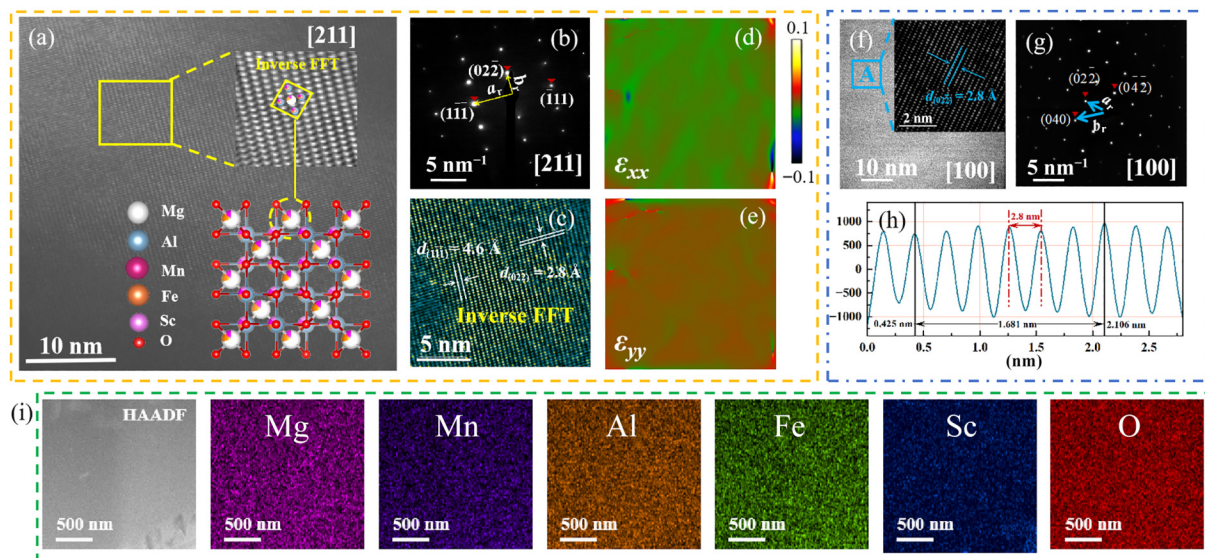


Fig. 2 Microstructural analysis of 3Sc-MMAFO ceramic. (a) HRTEM image and crystal structure viewed along $[211]$ zone axis; (b) SAED pattern; (c–e) IFFT and GPA analyses. (f, g) HRTEM image and SAED image along $[100]$ zone axis; (h) lattice fringe spacing from the blue box in (f); (i) EDS elemental mappings.

maximum, but as the Sc³⁺ substitution level gradually increases, the lattice mismatch gradually decreases as the secondary phase Sc₂O₃ separates, which leads to a decrease in the binding energy. The Sc 2p XPS peaks are significantly shifted to the right, which means that the binding energy reaches its maximum when $\gamma = 1$ and then decreases because of the precipitated Sc₂O₃. To analyze the oxygen vacancy concentration quantitatively, peak deconvolution of the O 1s XPS spectrum was performed. The O 1s peak of γ Sc-MMAFO was resolved into three components corresponding to lattice oxygen (O_L), oxygen vacancies (O_V), and surface adsorbed oxygen (O_A). Quantitative analysis revealed a decrease in the oxygen vacancy concentration from 25.71% to 16.58%. To verify the presence of oxygen vacancies and their variation trends, the samples were characterized by electron paramagnetic resonance (EPR). As shown in Fig. 3(e), the EPR signal intensity at $g = 2.0033$ progressively attenuated with increasing substitution content, confirming a reduction in the concentration of oxygen vacancies. This trend was further corroborated by low-temperature EPR measurements (Fig. S6 in the ESM).

3.2 NTC thermistor properties

The impedance spectrum (IS) of the γ Sc-MMAFO ceramics was measured over the temperature range of 323–773 K (Figs. 4(a) and 4(b) and Fig. S7(a) in the ESM). Notably, the Nyquist plots reveal three distinct impedance contributions: (1) a high-frequency intercept on the real impedance axis (Z') (inset of Fig. 4(a)), corresponding to the grain resistance (R_g); (2) semicircular arcs in the mid-frequency range, reflecting the grain boundary resistance (R_{gb}); (3) low-frequency arcs associated with electrode effects [38,39]. To analyze the high-frequency and low-frequency response characteristics more intuitively, we extracted R_g , R_{gb} , and the grain-boundary capacitance (Fig. S9 and Table S2 in the ESM) via the equivalent circuit model shown in Fig. S8 in the ESM. In the imaginary impedance Z'' - f spectra, the broadening of the Z'' peak profile with increasing temperature indicates the presence of a temperature-dependent dielectric relaxation mechanism (Fig. S7(b) in the ESM) [40].

The resistance–temperature curves exhibit typical NTC

behavior (shown in Fig. S7(c) in the ESM). All the samples show a consistent decrease in resistance as the temperature increases. The relationship between the natural logarithm of the resistivity ($\ln\rho$) and the reciprocal of the absolute temperature ($1000/T$) conforms to the Arrhenius equation (Fig. 4(c)), which can be described by Eq. (6) [41]:

$$\rho = \rho_0 \exp(B/T) = \rho_0 \exp(E_a/(kT)) \quad (6)$$

where ρ_0 is the resistivity at infinite temperature ($T \rightarrow \infty$); T is the absolute temperature; E_a is the activation energy for electrical conduction and can be calculated from the slopes of the $\ln\rho$ - $1000/T$ plots; k is the Boltzmann constant. As shown in Fig. 4(c), Sc³⁺ substitution significantly increases the slope of $\ln\rho$ - $1000/T$, which also indicates an increase in the hopping activation energy (E_a), as shown in Fig. 4(d). In this regard, the substitution of Sc³⁺ has a similar effect to the addition of other nonconductive ions, which essentially increases the difficulty of hopping small polarons [42,43].

Resistivity and the B value are significant parameters affecting NTC thermistor properties. Resistivity imposes no strict constraints, as device resistance can be geometrically tailored [44]. The B value, however, critically governs the thermistor sensitivity. This sensitivity is quantified by the temperature coefficient of resistance (α_T), which is defined by Eq. (2) and is directly proportional to the B value and has an inverse quadratic relationship with the temperature (T). Notably, α_T decreases significantly with increasing temperature. Consequently, achieving high sensitivity at elevated temperatures necessitates materials with high B values.

Figure 4(d) shows the B values of all the samples. The B values of the Sc³⁺-doped samples are significantly greater than those of the unmodified samples. On the basis of the analysis of the XPS data, the substitution of Sc³⁺ promoted the oxidation of Mn²⁺ to Mn³⁺ and the reduction of Fe³⁺ to Fe²⁺. The significant change in the ionic valence ratio leads to an increase in the activation energy of the polaron hopping, which in turn induces a synergistic increase in the resistivity and B values. The B values of the γ Sc-MMAFO ceramics over the corresponding temperature ranges

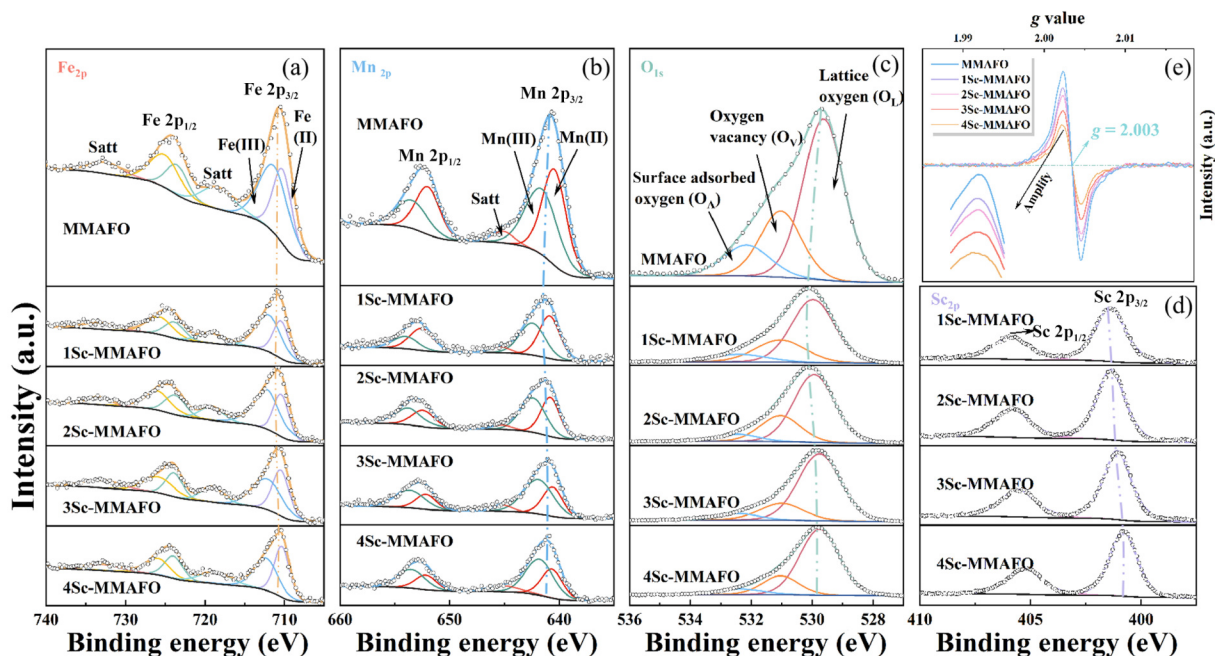


Fig. 3 XPS spectra of (a) Fe 2p, (b) Mn 2p, (c) O 1s, and (d) Sc 2p. (e) EPR spectra.

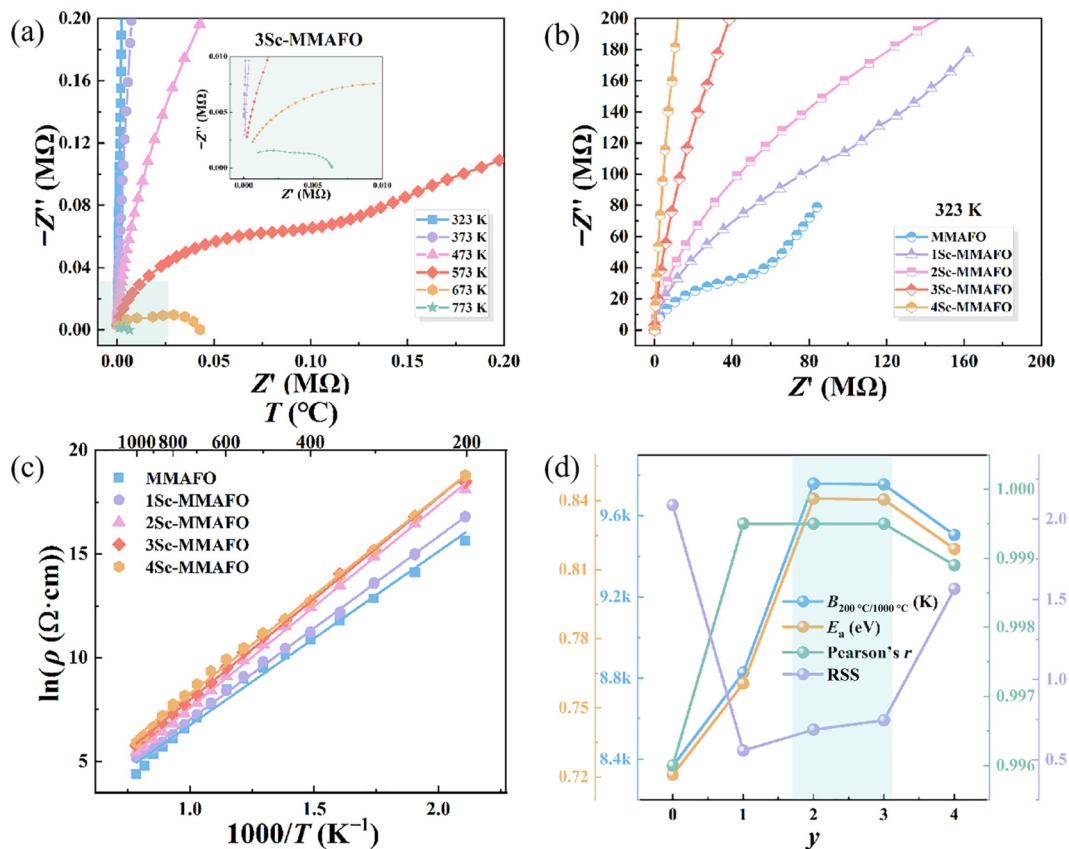


Fig. 4 NTC thermistor properties of ceramics. (a) IS of 3Sc-MMAFO ceramic measured between 323 and 773 K; (b) IS at 323 K; (c) relationship between $\ln\rho$ and $1000/T$; (d) linear fitting parameters: B , E_a , r , and RSS.

were calculated (Fig. S7(d) in the ESM). Notably, the 2Sc-MMAFO and 3Sc-MMAFO ceramics not only have a wider operating temperature range (200–1000 °C) but also higher B values (9758 and 9754 K) than the undoped sample does, ensuring a wider temperature range and higher temperature sensitivity. In addition, the linearity of the $\ln\rho$ – $1000/T$ curves for the Sc³⁺-substituted samples was significantly improved and optimized. Pearson's r increases from 0.9960 to 0.9995. For samples with $y = 2$ and 3, the relationship between $\ln\rho$ and $1000/T$ maintains excellent linearity even at temperatures as high as 1000 °C. These findings emphasize the efficacy of Sc³⁺ substitution in improving the linearity of thermistor materials.

3.3 Low-frequency dielectric behavior

To investigate the dielectric behavior of the ceramics, low-frequency dielectric measurements were systematically conducted over a wide temperature range of 25–400 °C, as shown in Fig. S10 in the ESM. As shown in Fig. 5(a), the ϵ_r curves of all the samples are approximately parallel to the x -axis (below 200 °C), indicating good stability of ϵ_r . In the low-frequency range, the $\tan\delta$ values remain below 0.016, among which the 3Sc-MMAFO sample has a minimal $\tan\delta$ of 0.0013 under the measurement conditions of 1 MHz and 50 °C.

Figure 5(b) shows the variation in ϵ_r with frequency at RT. ϵ_r decreases rapidly at low frequencies and finally reaches a constant frequency-independent point at 1 MHz, exhibiting typical dielectric behavior. This frequency-dependent behavior stems from the different contributions of the four polarization mechanisms in the material. At low frequencies, electron displacement, ion displacement, dipole orientation, and space-charge polarization collectively dominate the total

polarization [45]. With increasing frequency, however, the relaxation processes associated with defect dipoles and space-charge polarization can no longer follow the rapid variations in the applied electric field. Consequently, high-frequency polarization is governed solely by electron and ion displacement mechanisms [46]. Figure 5(b) also depicts the frequency dependence of $\tan\delta$. Oxygen vacancies generate space charges that form leakage currents at grain boundaries, leading to elevated $\tan\delta$ values at low frequencies. As the frequency increases, these charges cannot keep pace with the reversal of the applied electric field, resulting in a tendency toward lower saturation values [47].

3.4 Microwave dielectric properties

3.4.1 Dielectric constant

As shown in Fig. 5, ϵ_r gradually increases with the substitution of Sc³⁺ with high ionic polarizability ($\alpha(\text{Sc}^{3+}) = 2.81 \text{ \AA}^3$ vs. $\alpha(\text{Al}^{3+}) = 0.79 \text{ \AA}^3$). The ϵ_r of ceramics depends on internal factors (ionic polarizability and lattice vibration) as well as external factors (density and phase composition) [48,49]. To eliminate the effect of porosity on the ϵ_r of $y\text{Sc-MMAFO}$ ceramics, a correction formula was applied via Bosman and Havinga's correction formula, as shown in Eqs. (7) and (8):

$$\epsilon_{\text{cor}} = \epsilon_r(1 + 1.5P) \quad (7)$$

$$P = 1 - \rho_r \quad (8)$$

where ϵ_{cor} is the corrected dielectric constant, and P is the porosity percentage. In addition, to investigate the relationship between the dielectric constant and polarizability of materials, researchers have

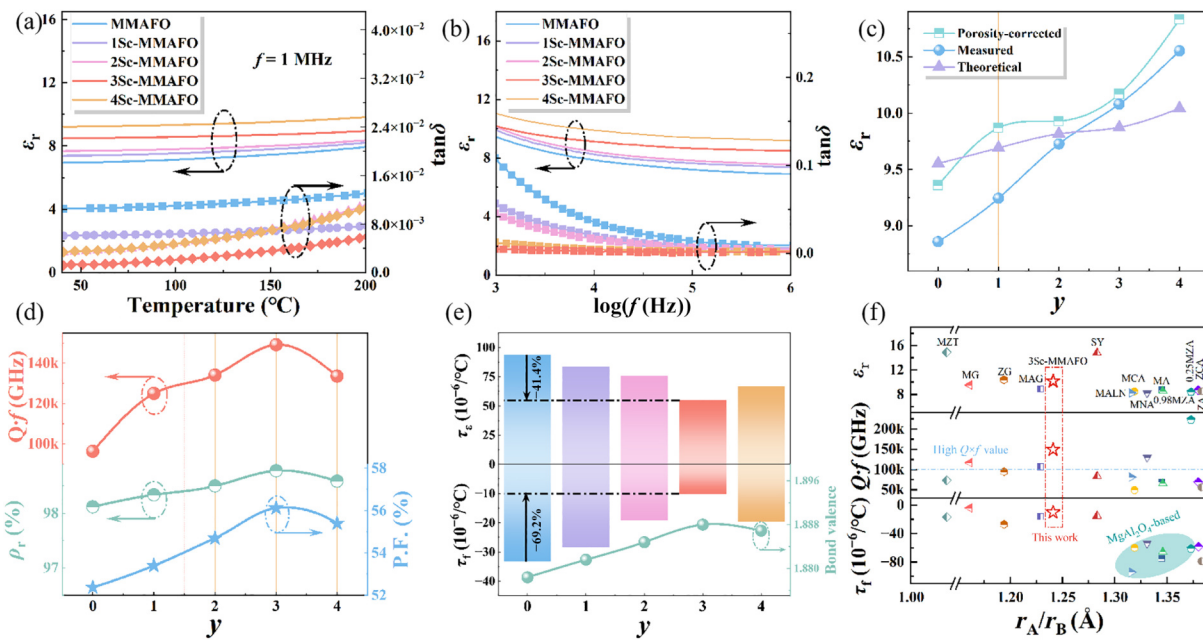


Fig. 5 Microwave dielectric properties of γ Sc-MMAFO ceramics. (a) Temperature dependence of ϵ_r and $\tan\delta$ at 1 MHz; (b) frequency dependence of ϵ_r and $\tan\delta$ at RT; (c) dielectric constant: ϵ_r , ϵ_{cor} , and ϵ_{theo} ; (d) Qf , ρ_r , and PF; (e) τ_f and τ_e ; (f) comparison of microwave dielectric properties of spinel-type ceramics, where r_A and r_B denote the equivalent ionic radii of the A-site and B-site, respectively.

proposed the concept of the theoretical dielectric constant (ϵ_{theo}) and calculated the value of ϵ_{theo} via the Clausius–Mosotti equation (Eq. (9)):

$$\epsilon_{theo} = \frac{3V_m + 8\pi\alpha}{3V_m - 4\pi\alpha} \quad (9)$$

where V_m is the molecular volume, and α is the polarizability of the γ Sc-MMAFO ceramics. The total ionic polarizability of γ Sc-MMAFO was predicted via Eq. (10):

$$\alpha_{theo} = \alpha(\text{Mg}^{2+}) + \alpha(\text{Mn}^{2+}) + (1-x)\alpha(\text{Al}^{3+}) + x\alpha(\text{Sc}^{3+}) + \alpha(\text{Fe}^{3+}) + 4\alpha(\text{O}^{2-}) \quad (10)$$

where $\alpha(\text{Mg}^{2+})$, $\alpha(\text{Mn}^{2+})$, $\alpha(\text{Al}^{3+})$, $\alpha(\text{Sc}^{3+})$, $\alpha(\text{Fe}^{3+})$, and $\alpha(\text{O}^{2-})$ are the ion polarizability values and can be obtained via the Shannon method [50] (as shown in Table S1 in the ESM). The calculated porosity-corrected and theoretical dielectric constants are shown in Fig. 5(c), which are consistent with the trends of the measured values. The small deviation between the theoretical and measured dielectric constants arises from the fact that the ion polarizability used in the calculations is an empirical parameter. Notably, the porosity-corrected ϵ_{cor} exceeds the measured values, which is attributed to the presence of pores in the actual microstructure, lowering the dielectric constant. The analysis demonstrated the dominant role of porosity (or density) in the macroscopic dielectric response of ceramics.

3.4.2 Qf

Figure 5(d) shows the variation in Qf , the packing fraction (PF), and the relative density as a function of the concentration of Sc³⁺. The PF is mainly used to describe cell space utilization, which is often considered a major factor affecting the Q value of microwave dielectric ceramics. Kim *et al.* [51] concluded that a higher PF leads to weaker vacancy scattering inside the crystal, which reduces loss in the system. Structural and atomic data were obtained for the samples through Rietveld refinement, from which PF was calculated via Eq. (11):

$$\text{PF} = \frac{\frac{4\pi}{3} \times (r_{(\text{Mg/Mn})}^3 + 2r_{(\text{Al/Sc/Fe})}^3 + 4r_{\text{O}}^3) \times Z}{V_{\text{cell}}} \quad (11)$$

where $r_{(\text{Mg/Mn})}$, $r_{(\text{Al/Sc/Fe})}$, r_{O} , and V_{cell} are the effective ionic radii at each coordination number and the unit cell volume, respectively. The experimental data reveal a strong positive correlation between PF and Qf , peaking simultaneously at $y = 3$ with PF = 56.12% and $Qf = 149,000$ GHz.

3.4.3 Temperature coefficient of resonant frequency

The structural features of the oxygen octahedron significantly affect the τ_f value. It is evident from Fig. 1(d) and Table S1 in the ESM that the unit cell volume increases and the average bond length of the Mn/Al/Sc/Fe–O bond decreases with increasing y . The change in bond length leads to a change in bond valence, and an increase in the bond valence at the B site usually leads to a decrease in the value of $|\tau_f|$, which is calculated via Eqs. (12) and (13) [52]:

$$V_{ij} = \sum_j v_{ij} \quad (12)$$

$$v_{ij} = \exp\left(\frac{R_{ij} - d_{ij}}{b'}\right) \quad (13)$$

where R_{ij} is the bond valence parameter, d_{ij} denotes the bond length between two atoms, and b' is a constant of 0.37 Å. Figure 5(e) shows that the value of τ_f follows the opposite trend of the bond valence. This is due to the increase in the lattice energy and tilt-restoring force of the oxygen octahedron with increasing bond valence, thus leading to a decrease in $|\tau_f|$.

Moreover, τ_f is related to the temperature coefficient of the dielectric constant (τ_e) and the linear coefficient of thermal expansion (α_L) [53]:

$$\tau_f = -\left(\frac{\tau_e}{2} + \alpha_L\right) \quad (14)$$

The α_L values of all the Sc^{3+} -substituted ceramics are close (as shown in Fig. S11 in the ESM), suggesting that τ_e plays a key role in regulating the magnitude of τ_f . The same tendency for τ_e and τ_f can be seen in Fig. 5(e).

3.4.4 Comparison of the microwave dielectric properties

Figure 5(f) shows the microwave dielectric properties of some spinel-type ceramics as a function of the ionic radius ratio at the A/B sites [18,19,54–65]. These spinel materials usually have low relative dielectric constants and high-quality factors, which are potentially valuable for applications in millimeter-wave signal propagation. The dielectric constants of the MgAl_2O_4 -based ceramics are basically stable in the range of 8–10, indicating that their properties are independent of the ionic radius. Compared with MgAl_2O_4 , the designed 3Sc-MMAFO ceramics have superior microwave dielectric properties ($\epsilon_r = 10.08$, $Qf = 149,000$ GHz, and $\tau_f = -10.2 \times 10^{-6} \text{ }^\circ\text{C}^{-1}$). These findings indicate that Sc^{3+} ion substitution is an effective way to improve the microwave dielectric properties of MgAl_2O_4 -based dielectric ceramics, which makes the developed dielectric ceramics promising for application in 5G/6G communication devices.

3.5 Design of CDRA

To validate the potential of ceramics for high-frequency applications, a 3Sc-MMAFO-based CDRA was developed, with the structural configuration and critical geometrical parameters detailed in Fig. 6(b). As depicted in Fig. 6(a), this CDRA functions as a millimeter-wave front-end module, achieving high gain, high radiation efficiency, directional beam control, and interference suppression capabilities in signal transmission. The test results indicate a center frequency of 12.01 GHz, bandwidth of 1.8 GHz (11–12.8 GHz), and reflection coefficient (S_{11}) of -35.66 dB (Fig. 6(c)). Operating in the Ku-band (12 GHz), this frequency

significantly enhances transmission speed and reliability in satellite communications, mobile wireless networks, and relay transmissions.

The deviation between the simulated and measured values likely originated from manufacturing tolerances and antenna impedance mismatch [66]. The maximum radiation efficiency reaches 92%, with a realized gain of 6.28 dBi (Fig. 6(d)). Figure 6(e) presents the 3D simulated radiation pattern, demonstrating the strongest electromagnetic signal radiation along the Z direction. The electric field (y-axis polarization) and magnetic field (semicircular distribution in the xoy-plane) profiles (Fig. 6(f)) confirm the dominant HE_{116} hybrid mode, which optimizes the broadside radiation in CDRA. The antenna radiation pattern at 12.01 GHz is shown in Fig. 6(g), where the copolarized field intensity exceeds the cross-polarized intensity along the apparent axis ($\theta = 0^\circ$). The 3Sc-MMAFO CDRA exhibits dual functionality as both a high-Q resonator ($Qf = 149,000$ GHz) and a high-B thermistor sensor ($B_{200/1000^\circ\text{C}} = 9754$ K), enabling self-temperature-compensated RF modules for 6G millimeter-wave massive MIMO base stations.

4 Conclusions

In conclusion, this study presents a systematic study of Mg–Al–Mn–Fe–O spinel ceramics for multifunctional devices. The results demonstrate that the 3Sc-MMAFO ceramic displays NTC thermistor properties across an extended temperature range (200–1000 $^\circ\text{C}$), with a B value of 9754 K, ensuring measurement accuracy and temperature sensitivity. In addition, the optimized 3Sc-MMAFO ceramic simultaneously achieves superior microwave dielectric properties with $\epsilon_r = 10.08$, $Qf = 149,000$ GHz, and $\tau_f = -10.2 \times 10^{-6} \text{ }^\circ\text{C}^{-1}$. Significantly, the developed 3Sc-MMAFO-based resonant antenna demonstrates practical applicability in millimeter-wave systems, operating at 11–

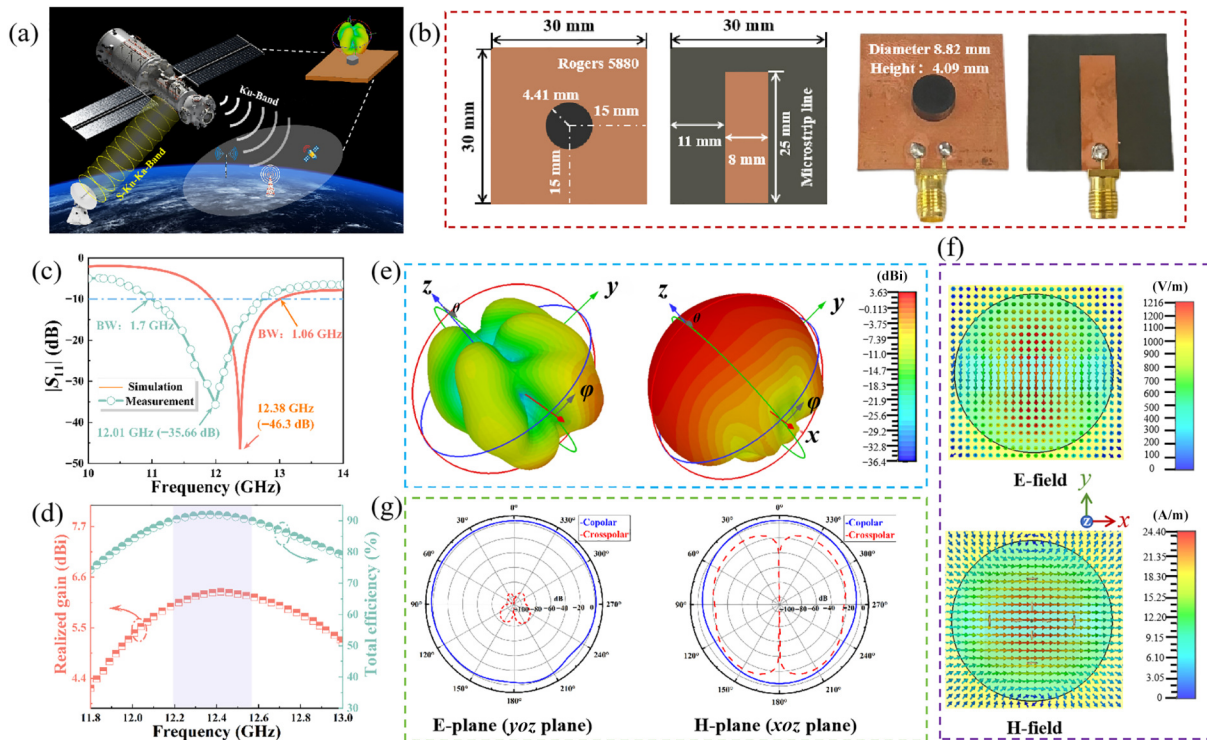


Fig. 6 Antenna design and performance analysis. (a) Schematic diagram of application prospects of resonator antenna; (b) antenna dimensions and design; (c) simulated and measured return loss S_{11} of proposed antenna; (d) simulated antenna radiation efficiency and realized gain; (e) 3D simulated radiation patterns of copolarized and cross-polarized; (f) simulation results of electric field and magnetic field; (g) simulation results of radiation pattern in E and H planes.

12.8 GHz with 92% radiation efficiency and 6.28 dBi realized gain. Ultimately, these comprehensive functional properties establish the 3Sc-MMAFO ceramic as a promising dual-functional material for microwave-thermosensitive integrated devices.

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Availability of data and materials

The data that support the findings of this study are available from the corresponding author upon reasonable request.

Competing interests

The authors have no competing interests to declare that are relevant to the content of this article.

Electronic Supplementary Material

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