

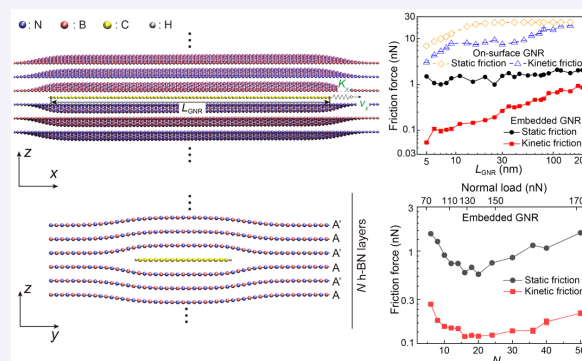
Robust superlubricity in encapsulated graphene nanoribbons through van der Waals confinement

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ABSTRACT: The frictional behavior of encapsulated graphene nanoribbons is pivotal for enabling ultralong growth and ensuring the reliability of nanoelectronic devices, yet it remains elusive due to the buried nature of the interfaces. Using large-scale molecular dynamics simulations, we demonstrate that GNRs confined between hexagonal boron nitride (h-BN) layers exhibit friction forces over an order of magnitude lower than those of their on-surface counterparts. The kinetic friction force (F_k) scales sublinearly with length (L_{GNR}) as $F_k \propto (\ln(L_{\text{GNR}}))^3$. This robust superlubric state originates from interfacial registry competition with adjacent AA'-stacked h-BN layers, which inhibits coherent strain accumulation and suppresses stick-slip behavior, thereby promoting collective low-dissipation sliding. Furthermore, we reveal a negative differential friction coefficient versus confinement pressure as the number of h-BN layers increases, arising from the competition between pressure-induced ripple suppression and the monotonically enhanced h-BN/h-BN interlayer perturbations in thicker stacks. This interplay provides a practical avenue for tuning friction via confinement engineering. These findings elucidate atomistic dissipation pathways at buried van der Waals interfaces and establish encapsulation as a viable route to robust GNR-based nanoelectronics and scalable superlubric systems.

KEYWORDS: van der Waals (vdW) encapsulation; graphene nanoribbon (GNR); superlubricity; friction scaling law; interfacial registry competition



1 Introduction

Graphene nanoribbons (GNRs) exhibit exceptional electronic [1, 2] and mechanical properties [3], making them promising building blocks for nanoelectronic devices such as field-effect transistors (FETs), quantum circuits, flexible electronics, sensors, and thermoelectric generators [4–11]. However, despite progress in fabrication methods such as top-down cutting [12, 13], nanotube unzipping [14, 15], bottom-up chemical vapor deposition [6, 16–21], and on-surface synthesis [22–24], these approaches typically produce ribbons with a trade-off between length and width, poor chirality control, and structural nonuniformity [25–27], limiting their integration into high-performance devices. A recent breakthrough by Lyu et al. [28, 29] demonstrated the *in situ* growth of ultralong (0.25 mm), ultranarrow (< 5 nm), and homochiral zigzag (ZZ) GNRs within hexagonal boron nitride (h-BN) stacks. This approach enabled the transfer-free fabrication of embedded GNR FETs with outstanding performance—mobilities up to $\sim 4,600 \text{ cm}^2 \text{ V}^{-1} \text{ s}^{-1}$ and on/off ratios of $\sim 10^6$. This advance not only stimulated broad

interest and attention [30–34] but also revealed that the friction at the embedded interface is a decisive factor controlling ultralong growth and chirality selection.

Although the tribological behavior of surface-supported GNRs has been extensively studied, including superlubricity [35, 36], edge effects [36], length dependence [37–39], and morphological evolution [40], the frictional behavior of fully encapsulated GNRs remains largely unexplored. Unlike surface-supported ribbons, an encapsulated GNR is simultaneously in contact with two adjacent layers, where van der Waals (vdW) confinement can fundamentally alter the mechanical [41–43], frictional [44–46], electronic [47–50], and thermal transport [51–55] behavior of layered heterostructures and related devices. Frictional forces at embedded interfaces can drive wear, strain accumulation, and dissipation while also strongly coupling to electronic and thermal transport [56–61]. Clarifying the microscopic mechanisms of encapsulated GNR friction is therefore essential for advancing fundamental tribology as well as for enabling the design of reliable nanoscale devices [62–66] and the aforementioned homochiral ultralong GNR growth.

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In this work, we employ large-scale molecular dynamics (MD) simulations with state-of-the-art force fields [67, 68] to systematically investigate the frictional behavior of GNRs embedded between h-BN layers. We show that encapsulation reduces friction by over an order of magnitude compared with surface-supported GNRs. Furthermore, we identify a consistent slow sublinear scaling of friction with nanoribbon length that persists across a wide range of sliding velocities, confirming the manifestation of robust superlubricity. This ultralow friction state originates from registry competition with adjacent AA'-stacked h-BN layers, which suppresses strain accumulation and prevents localized stress, enabling smooth collective sliding instead of soliton-mediated stick-slip. Finally, we demonstrate that the number of h-BN encapsulation layers provides a practical route to tune friction through vdW confinement pressure. Together, these findings establish encapsulation as a powerful mechanism for achieving controllable superlubricity, clarify the role of buried interfaces in enabling ultralong GNR growth, and provide design principles for robust, durable, and energy-efficient GNR-based nanoelectronic systems.

2 Model setup

Our model system consists of armchair (AC)- and zigzag (ZZ)-GNRs encapsulated within six layers of AA'-stacked h-BN (Fig. 1). The GNRs were aligned along the AC (ZZ) direction of the h-BN lattice for AC-GNRs and ZZ-GNRs, with lengths (L_{GNR}) ranging from 5 to 200 nm and a fixed width of ~ 2 nm. The ribbons were passivated with hydrogen at the edges. Periodic boundary conditions were applied in the x and y directions, while an open boundary condition was used in the z direction, with a 2 nm vacuum spacing. The lateral dimensions of the simulation box were set as $(L_{\text{GNR}} + 8)$ nm $\times$ 12 nm to avoid interaction between periodic images.

The intralayer interactions within the GNR and h-BN layers were described using the second-generation reactive empirical bond order (REBO) potential [69] and the Tersoff potential [70], respectively. Interlayer interactions, including those between h-BN layers and between GNR and h-BN, were described via the registry-dependent interlayer potential (ILP) [39, 68, 71–74] with refined parameterization [39]. This state-of-the-art ILP captures the registry-dependent sliding energy corrugation by explicitly accounting for short-range Pauli repulsion [68], making it the current tool-of-choice for describing the anisotropic nature of weak and long-range vdW interactions in layered systems. The ILP has been extensively validated across various vdW heterostructures for characterizing structural reconstruction [47, 72, 75], thermal transport [51–53], mechanical [71, 76], and frictional [67, 77, 78] properties, as well as for simulating the growth of quasi-one-dimensional materials [28, 79]. While these empirical hybrid force fields perform robustly for pristine lattices,

we acknowledge that their accuracy may decrease in nonideal systems featuring edges or defects. Such limitations could be addressed in future work by adopting a hybrid framework that combines single-layer machine-learned potential (sMLP) with a reparameterized ILP [80]. All simulations were carried out using the large-scale atomic/molecular massively parallel simulator (LAMMPS) package [81].

Prior to the sliding friction simulations, the system was fully relaxed to eliminate residual stress from GNR insertion. The whole system was equilibrated at 10 K and zero pressure for 100,000 steps with a time step of 1 fs, where the pressure was controlled by the Nosé-Hoover barostat. Then, the system was further optimized using the fast inertial relaxation engine (FIRE) algorithm with a threshold force value of 10^{-6} eV·Å $^{-1}$, followed by 10 iterative cycle combinations of the conjugate gradient (CG) and box/relax algorithm with a force convergence criterion of 10^{-4} eV·Å $^{-1}$. A final optimization using the FIRE algorithm was performed with a threshold force value of 10^{-6} eV·Å $^{-1}$. This relaxation induced a spindle-shaped deformation of the h-BN layers, where the layers are locally pushed apart by the presence of the GNR and then gradually recover their equilibrium interlayer spacing (~ 3.3 Å) at regions away from it (Fig. 1), consistent with previous experimental observations [28].

Subsequently, damped sliding friction simulations were carried out at 0 K under the NVE ensemble with a time step of 1 fs. The rightmost carbon atoms of the GNR were connected to a driving stage via parallel lateral springs, where the stage moved at a constant velocity of $V_x = 1$ m·s $^{-1}$ along the x direction. The overall spring stiffness was fixed at $K_x = 100$ N·m $^{-1}$ [82], yielding an atomic spring constant of $k_x = K_x/n$ for each dragged spring, where n is the total number of dragged atoms. Tests with a reduced stiffness of 30 N·m $^{-1}$ confirmed that the qualitative frictional behavior remained unchanged (Fig. S1 in the Electronic Supplementary Material (ESM)). The far-edge regions of the h-BN slab (highlighted by red boxes in Fig. 1(a)) were held fixed as rigid boundaries. To dissipate heat generated during sliding, a Langevin thermostat damping ($\eta = 1$ ps $^{-1}$) was applied to the atoms in the outermost h-BN layers (top layer L6 and bottom layer L1 in Fig. 1(b)) [83–85]. The lateral spring force on each dragged carbon atom is given by Eq. (1):

$$F_i(t) = k_x (x_i(t) - X^{\text{stage}}(t)) \quad (1)$$

where $X^{\text{stage}}(t)$ and $x_i(t)$ are the instantaneous position of the driving stage and the i^{th} carbon atom in the driving GNR edge, respectively. The total lateral force acting on the GNR was then calculated as $F_L(t) = \sum_{i=1}^n F_i(t)$.

For comparison, we also performed friction simulations of on-surface GNRs using the same setup, except that the top h-BN trilayer stack was removed and only the bottom h-BN layer was thermostatted (Fig. S2 in the ESM). Furthermore, we performed

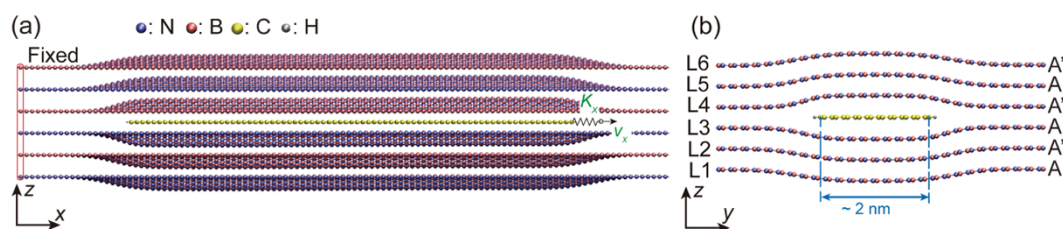


Fig. 1 MD simulation model and setup. (a) Side view along the y direction of the embedded GNR system, where a GNR is encapsulated by six AA'-stacked h-BN layers. The atoms in the red highlighted regions are fixed during sliding. (b) Cross-sectional view along the x direction of the simulation model. The rightmost carbon atoms of the GNR were attached via springs to a stage moving at a constant velocity $V_x = 1$ m·s $^{-1}$. The width of the GNR is fixed at ~ 2 nm, while its length varies from 5 to 200 nm. Mauve, blue, yellow, and gray spheres represent boron, nitrogen, carbon, and hydrogen atoms, respectively.

friction simulations for 30-nm-long GNRs embedded between h-BN stacks of varying thicknesses using the same setup as the six-layer system. In all these thickness-dependent simulations, the damping layers were consistently applied to the topmost and bottommost h-BN layers.

3 Results and discussion

Figure 2(a) shows representative lateral force traces for an embedded h-BN/GNR/h-BN ($L_{\text{GNR}} = \sim 71$ nm) system, revealing that AC-GNRs undergo stick-slip motion, whereas ZZ-GNRs exhibit smooth sliding, both with a characteristic period of ~ 2.3 Å (Fig. S3 in the ESM). The kinetic friction force was obtained by averaging the lateral force over multiple steady-state sliding periods, while the maximum lateral force over the entire trace was defined as the static friction force. Statistical errors in the kinetic friction were estimated from ten independent data sets, each spanning one sliding period. The kinetic friction (0.35 nN) of the embedded ZZ-GNR is ~ 1.5 times smaller than that of its AC-GNR counterparts (0.55 nN), consistent with our earlier findings [28]. This difference originates from the larger lateral displacements and greater deformation experienced by the AC-GNR as it navigates around local high-energy barriers (Section S4 in the ESM for details). Representative lateral force traces for on-surface GNRs ($L_{\text{GNR}} = \sim 71$ nm) are presented in Fig. 2(b). Both AC- and ZZ-GNRs exhibit pronounced stick-slip behavior, with nearly identical kinetic friction forces (12.9 nN for AC-GNRs and

13.4 nN for ZZ-GNRs). The sliding dynamics closely resemble those reported in our previous work [39]. Importantly, both the static and kinetic friction forces of on-surface GNRs are over an order of magnitude higher than those of embedded GNRs.

To further elucidate the interfacial frictional behavior of embedded GNRs, we investigate the dependence of the static and kinetic friction forces on the ribbon length (L_{GNR}) for both AC-GNRs and ZZ-GNRs. As demonstrated in Figs. 2(c) and 2(d), both forces increase sublinearly with L_{GNR} in the range of 5–200 nm. The static friction approximately doubles for AC-GNRs (red curves) and triples for ZZ-GNRs (black curves), following a scaling relation of $\sim 0.6(L_{\text{GNR}}/L_0)^{0.25}$, where $L_0 = 1$ nm. The kinetic friction (F_k) rises from ~ 0.1 to ~ 0.8 nN for both edge types, following the scaling law:

$$F_k \approx 0.005(\ln(1 + L_{\text{GNR}}/L_0))^3 \quad (2)$$

Notably, the static friction of embedded GNRs exhibits periodic oscillations with length, arising from incomplete moiré patterns at the ribbon edges [86].

In contrast, on-surface GNRs display friction forces that are consistently over an order of magnitude higher. Their static friction (blue and orange curves in Fig. 2(c)) grows linearly with length before saturating beyond $L_{\text{GNR}} \approx 20$ nm, reaching plateaus of ~ 22.5 nN for the AC-GNRs and ~ 20.7 nN for the ZZ-GNRs. The kinetic friction (blue and orange curves in Fig. 2(d)) continues to increase with length, rising from ~ 2 up to ~ 16 nN for

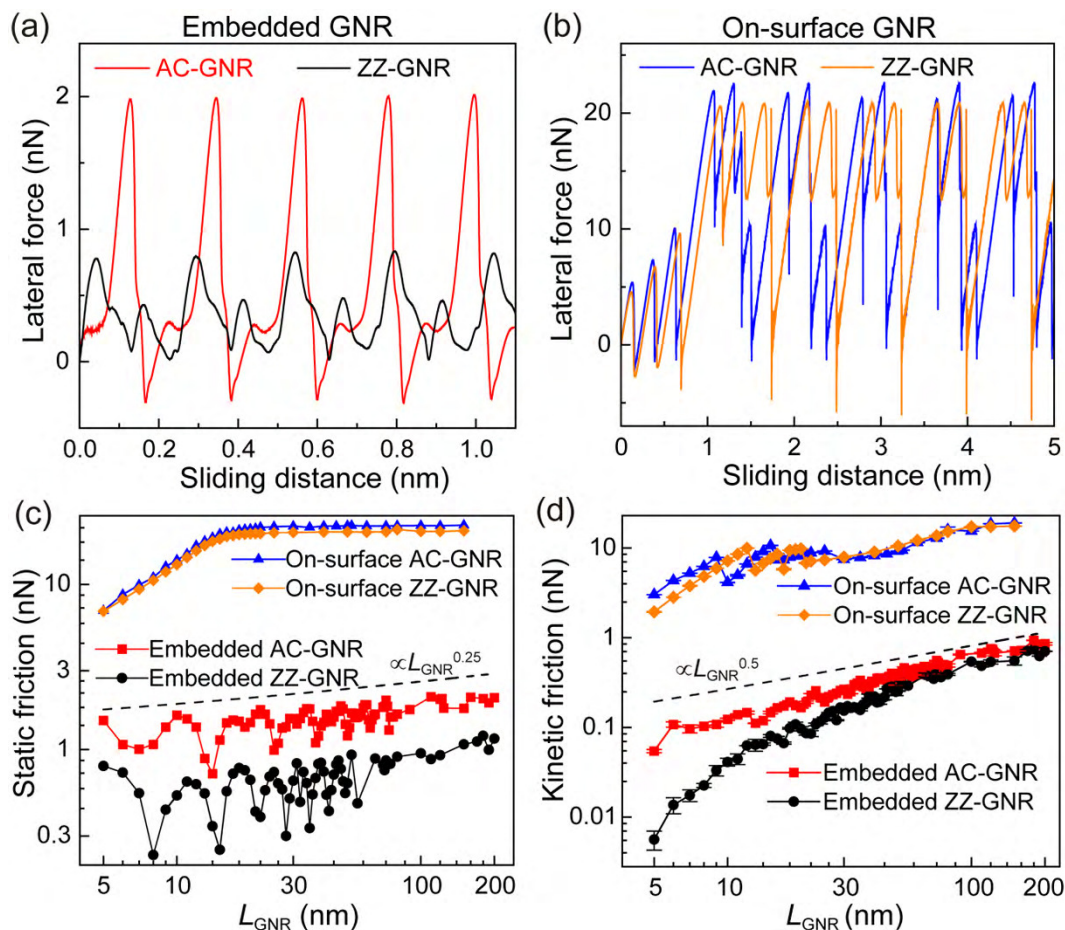


Fig. 2 Lateral force traces and length dependence of friction forces. Typical lateral force traces for (a) embedded and (b) on-surface GNRs with a length of ~ 71 nm. (c) Static and (d) kinetic friction forces of embedded and on-surface AC-GNRs and ZZ-GNRs with different L_{GNR} . The dashed lines indicate sublinear power-law scaling of friction with length.

both AC- and ZZ-GNRs, with a scaling law of $\sim 1.5(L_{\text{GNR}}/L_0)^{0.5}$. Extrapolation of the above scaling laws predicts an intersection of the static friction of embedded and on-surface GNRs at a ribbon length of $\sim 1,400 \mu\text{m}$, whereas the kinetic friction of embedded GNRs increases more slowly with length than that of on-surface GNRs and therefore remains consistently lower. These results highlight that h-BN encapsulation yields robust superlubricity in h-BN/GNR/h-BN heterostructures compared to their on-surface counterparts.

To investigate the effects of sliding velocity and temperature on frictional behavior, additional simulations were performed at both 0 K and room temperature under driving velocities of 0.5, 2, and $5 \text{ m}\cdot\text{s}^{-1}$, as well as under quasi-static conditions. These tests confirm that the frictional trends reported for $V_x = 1 \text{ m}\cdot\text{s}^{-1}$ are preserved across the explored velocity range at both temperatures (Figs. S6–S8 in the ESM). Notably, both the static and kinetic friction forces of the GNR increase with sliding velocity but decrease with rising temperature due to thermal activation effects. Despite these variations, the embedded h-BN/GNR/h-BN system maintains its robust superlubric state under all conditions

examined (Figs. S6–S8 in the ESM). Collectively, these results indicate that our findings obtained at 0 K and $V_x = 1 \text{ m}\cdot\text{s}^{-1}$ are relevant and applicable to realistic experimental scenarios. Further simulations with varying ribbon geometries and chiralities, including AC-GNRs with widths of $w = 0.7$ and 4.1 nm (Fig. S9 in the ESM), as well as atomically precise chiral GNRs with indices (3, 1, 8) [87, 88] (Fig. S10 in the ESM), reveal that while the friction magnitudes may vary with geometry and edge structure, the fundamental frictional scaling behavior remains preserved across all cases.

To elucidate the origin of the distinct sliding frictional behaviors in embedded and on-surface GNR systems, we analyzed the evolution of stress and strain distribution along the sliding direction (σ_{xx} and ϵ_{xx}) together with the bond-length evolution, displacement dynamics, and local registry index (LRI) [89, 90], using a 71-nm-long AC-GNR as a representative case (Fig. 3 and Figs. S12–S16 in the ESM). Here, σ_{xx} and ϵ_{xx} characterize the deformation of the GNR along the sliding direction, while the LRI quantifies the degree of local commensurability between the GNR and the h-BN layers, with lower values indicating stronger

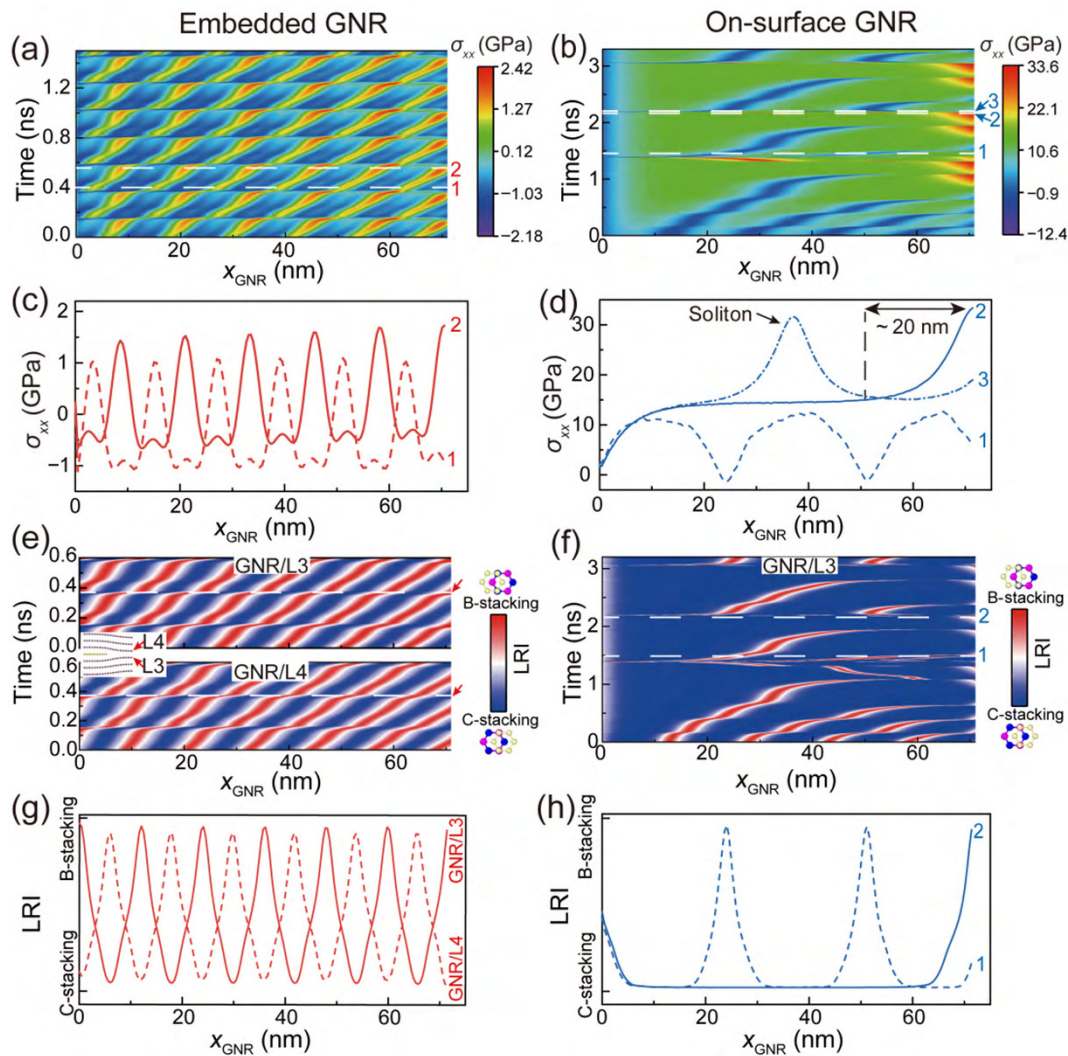


Fig. 3 Stress and registry evolution of embedded and on-surface AC-GNRs. (a, b) Stress distribution (σ_{xx}) of a $\sim 71 \text{ nm}$ long (a) embedded and (b) on-surface GNR during sliding. (c, d) Cross-sectional profiles along the dashed lines in panels (a) and (b). Panel (d) highlights the localized tensile stress near the leading edge, with a characteristic penetration length of $\sim 20 \text{ nm}$, as well as the emergence of a stress soliton. (e, f) Local registry index (LRI) evolution for the embedded GNR with adjacent h-BN layers L3 and L4 (the positions of L3 and L4 are indicated in the inset of panel (e)). (g, h) Cross-sectional LRI profiles along the dashed lines in panels (e) and (f). Panel (g) illustrates the registry dislocation between GNR/L3 and GNR/L4. Both σ_{xx} and LRI are calculated by averaging the per-atom stress/LRI values along the narrow dimension of the GNR (excluding the passivating hydrogen atoms) and over a single axial unit cell. The position of each axial unit cell along the GNR (x_{GNR}) is calculated as the distance of its center-of-mass from the trailing edge of the ribbon. See more details in Section S8 of the ESM.

commensuration. Further calculation details are provided in Section S8 in the ESM.

In the encapsulated GNR configuration, σ_{xx} and ϵ_{xx} at the leading edge rise only slightly during sliding and decay smoothly and nearly linearly toward the trailing edge (Figs. 3(a) and 3(c) and Figs. S12 and S13 in the ESM). This nearly uniform stress distribution originates from registry competition between the GNR and the two adjacent AA'-stacked h-BN layers (L3 and L4 marked in the inset of Fig. 3(e)), as shown in Figs. 3(e) and 3(g) and Fig. S14 in the ESM. The GNR can align with the upper layer only by misaligning with the lower layer, and vice versa. This continual dislocation prevents the GNR from achieving full commensuration with either interface, thereby limiting elastic strain accumulation. As a result, the embedded GNR undergoes collective sliding with only minor fluctuations, accompanied by transient moiré patterns at the edges (Movie S1 and Figs. S15 and S16 in ESM). The total sliding barrier (ΔE_{tot}) remains low and is dominated by small variations in interlayer potential energy (ΔE_{int}) rather than stored elastic strain energy ($\Delta E_{\text{el}}^{\text{GNR}}$) (Fig. S17 and Table S1 in the ESM). Consequently, embedded GNRs exhibit ultralow, gradually increasing friction without saturation in the studied length range.

In contrast, a GNR sliding on a single-sided h-BN substrate develops a sharp stress and strain concentration at the leading edge, with σ_{xx} reaching 33.6 GPa (Figs. 3(b) and 3(d) and Figs. S12 and S13 in the ESM). Sliding proceeds via soliton-mediated stick-slip events, accompanied by pronounced tail-swing dynamics (Fig. 3(d) and Movie S2 in the ESM), consistent with earlier studies [38, 91, 92]. During the stick phase, C-C bonds stretch from the equilibrium 1.42 Å to 1.436 Å across most of the ribbon and up to 1.459 Å at the leading edge (Fig. S15 in the ESM). This elongation reduces the lattice mismatch with the substrate (the equilibrium B-N bond length is 1.446 Å) and promotes local commensuration (Figs. 3(f) and 3(h) and Fig. S14 in the ESM). This process enables substantial elastic energy storage while the leading edge advances and the trailing edge remains pinned (Fig. S16 in the ESM), which is abruptly released during slip events (Figs. 3(b) and 3(d) and Figs. S12 and S13 and Movie S2 in the ESM). The corresponding ΔE_{tot} is thus an order of magnitude higher than in the embedded case (Fig. S17 and Table S1 in the ESM), indicating the dominance of strain energy over interlayer potential variations. Stress relaxation follows an exponential decay with a characteristic penetration length of ~20 nm. For ribbons longer than this threshold, static friction saturates because only the leading segment of the GNR resists motion. For shorter GNRs, stress decays linearly from the leading to the trailing edge rather than forming a localized concentration (Fig. S20 in the ESM), leading to a linear friction-length relation.

Overall, embedded GNRs achieve smooth, low-friction sliding by suppressing stress localization through interfacial registry competition. In contrast, on-surface GNRs accumulate localized strain, which leads to higher static and kinetic friction, pronounced stick-slip oscillations, and soliton-driven slip events. This difference in strain accumulation drives distinct evolutions of the moiré pattern (Fig. S17 in the ESM). However, the Moiré evolution is a geometric manifestation of changing local registry, not an independent source of friction (Section S10 in the ESM). Moreover, no interfacial covalent bonding forms between the GNR and h-BN layers (Fig. S19 in the ESM).

To better understand the kinetic friction contrast between embedded and on-surface configurations, we analyzed the system's energy dissipation and its directional decomposition (Section S12 for details). The real-time dissipation power of atom j in the dissipative h-BN layers is calculated as Eq. (3):

$$p_{\text{diss},\alpha}^j(t) = \eta m_j (v_{\alpha}^j(t))^2, m_j = m_{\text{B}} \text{ or } m_{\text{N}} \quad (3)$$

where $v_{\alpha}^j(t)$ is the velocity component of atom j in direction α ($\alpha = x, y, z$), η is the damping coefficient, and m_{B} and m_{N} are the atomic masses of boron and nitrogen atoms, respectively. The total instantaneous dissipation power of atom j is given by Eq. (4):

$$p_{\text{diss}}^j(t) = \sum_{\alpha=x,y,z} p_{\text{diss},\alpha}^j(t) \quad (4)$$

By averaging $p_{\text{diss}}^j(t)$ over multiple sliding periods, the time-averaged energy dissipation power $\langle p_{\text{diss}}^j \rangle$ is obtained. The total real-time dissipation power of the entire system and its directional dissipation components are expressed as Eq. (5):

$$P(t) = \sum_{j=1}^{n_{\text{diss}}} p_{\text{diss}}^j(t) \quad (5)$$

where n_{diss} is the total number of atoms in the damping layers. The time-averaged total dissipation power $\langle P \rangle$ and its directional components $\langle P_{\alpha} \rangle$ were obtained by averaging multiple sliding periods at the steady state.

Dissipation in embedded GNRs is overwhelmingly out-of-plane, whereas in on-surface GNRs, it is distributed across both out-of-plane (z) and in-plane (x, y) channels (Fig. S21 in the ESM). Mechanistically, embedded GNRs dissipate energy via moiré creep driven by out-of-plane relaxation, while on-surface GNRs exhibit mixed in-plane/out-of-plane dissipation associated with the formation and release of strain solitons (Fig. S22 and Movies S1 and S2 in the ESM). Phonon-spectrum analysis further supports this picture (Fig. S23 in the ESM). The embedded system dissipates primarily through low-frequency, out-of-plane washboard modes, characterized by the washboard frequency $f_{\text{wb}} = V_x/a$ [93–95], where a is the lattice constant of h-BN along the armchair direction. In contrast, the on-surface system activates a broader spectrum of higher-frequency in-plane and out-of-plane modes associated with solitonic edge dynamics and vigorous interfacial rearrangements.

The length dependence of kinetic friction in both configurations stems from how the dissipation region scales with ribbon size. The spatial distribution of the time-averaged per-atom dissipation power $\langle p_{\text{diss}}^j \rangle$ of the damped layers [96, 97] reveals that energy is mainly dissipated in the h-BN layers beneath the GNR, with pronounced hotspots near the GNR edges (Fig. S22 in the ESM). This feature is common to both on-surface and embedded configurations. As the ribbon length increases, more atoms participate in dissipation, and the total kinetic friction rises nearly proportionally with length. In short, longer GNRs generate larger dissipation regions, leading to higher overall friction.

For embedded GNRs, the h-BN encapsulation layers exert a vdW pressure arising from a balance between interlayer vdW interactions and elastic deformation of both the GNRs and the h-BN stack [98–101]. This pressure increases with the number of h-BN encapsulation layers (N), as shown in Fig. S24 in the ESM. To assess its effect on friction, we performed friction simulations for 30-nm-long GNRs embedded between h-BN stacks of varying thickness. The results reveal a nonmonotonic dependence of friction on N : Both static and kinetic friction decrease initially, reaching a minimum at ~16 layers, and then rise again (Figs. 4(a) and 4(b)). Specifically, the kinetic friction drops by ~54% for AC-GNRs (from ~0.26 to ~0.12 nN) and by ~67% for ZZ-GNRs (from ~0.15 to ~0.05 nN) as N increases from 6 to 16 (with the vdW encapsulation normal load increasing from ~80 to ~130 nN). Beyond this point, further encapsulation gradually

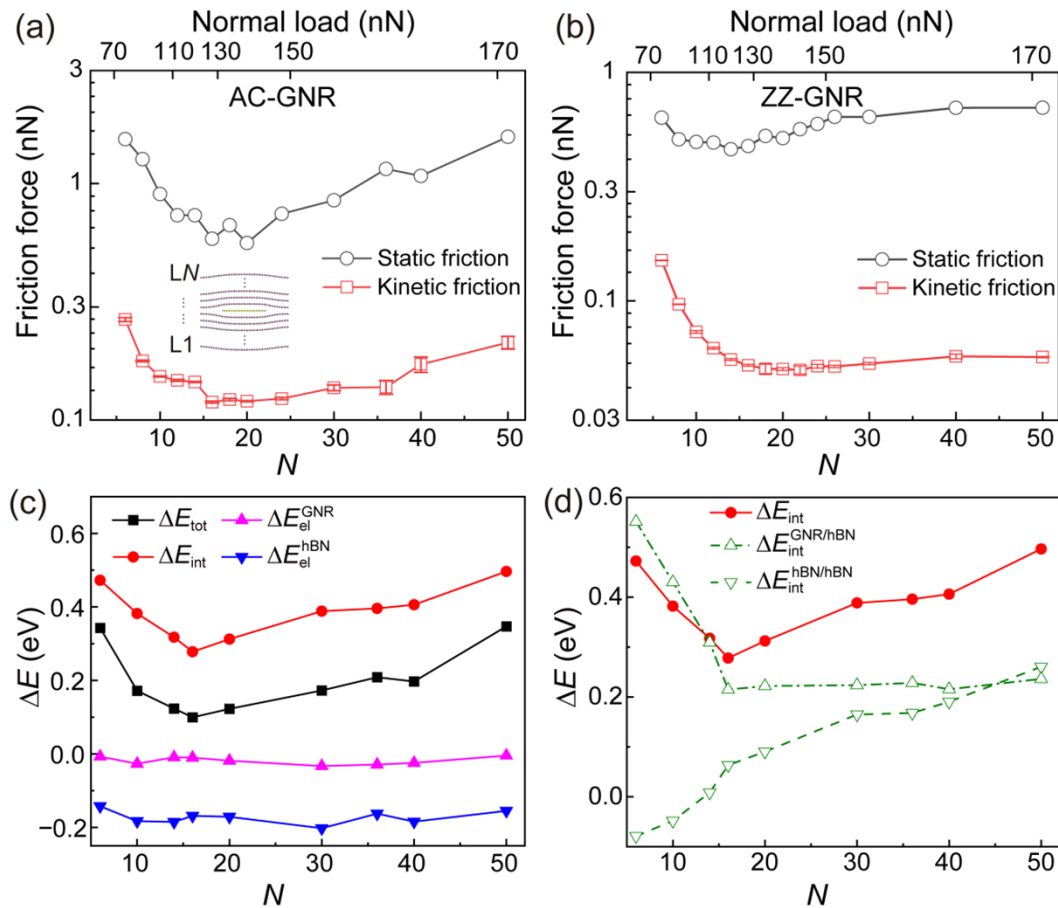


Fig. 4 Friction modulation in embedded GNRs by h-BN encapsulation thickness. (a, b) Static (black circle) and kinetic (red square) friction forces for embedded (a) AC-GNRs and (b) ZZ-GNRs as a function of the number of h-BN layers (N). The top axis indicates the corresponding normal load exerted by the encapsulation stack. The inset in (a) shows a side view of the simulation model. (c) Energy barrier of embedded AC-GNRs and their decomposition into the interlayer term (ΔE_{int}) and the intralayer elastic contributions from GNRs ($\Delta E_{\text{el}}^{\text{GNR}}$) and h-BN stack ($\Delta E_{\text{el}}^{\text{hBN}}$). (d) Further decomposition of ΔE_{int} into GNR/h-BN interfacial contributions ($\Delta E_{\text{int}}^{\text{GNR/hBN}}$) and h-BN/h-BN ($\Delta E_{\text{int}}^{\text{hBN/hBN}}$) interlayer interaction contributions.

increases friction, reaching ~ 0.21 nN (AC-GNR) and ~ 0.06 nN (ZZ-GNR) at 50 layers (with a vdW encapsulation normal load of ~ 175 nN). The corresponding differential friction coefficients (μ_k), obtained from a numerical two-point derivative of the kinetic friction with respect to the normal load, remain in nearly all cases within the superlubric regime ($\mu_k < 0.001$) [102], as shown in Fig. S25 in the ESM.

This non-monotonic trend results from competition between two opposing mechanisms. On the one hand, increased vdW pressure at higher N flattens the GNR by suppressing out-of-plane ripples induced by the $\sim 1.8\%$ lattice mismatch between GNR and h-BN [76, 96] (Fig. S26 in the ESM). This flattening reduces the variation in the GNR/h-BN interaction energy ($\Delta E_{\text{int}}^{\text{GNR/hBN}}$) during sliding, thereby lowering the total energy barrier (ΔE_{tot}) and friction. On the other hand, thicker h-BN stacks involve more h-BN/h-BN interlayer pairs perturbed during sliding, which monotonically increases the associated interaction energy variation ($\Delta E_{\text{int}}^{\text{hBN/hBN}}$) and raises ΔE_{tot} (Fig. S27 in the ESM). These mechanisms are quantified by decomposing ΔE_{tot} . While the elastic contributions from the GNR and h-BN remain nearly constant, the interlayer term ΔE_{int} mirrors the non-monotonic friction trend (Fig. 4(c)). Its components show opposing dependencies: $\Delta E_{\text{int}}^{\text{GNR/hBN}}$ decreases and then saturates with increasing N , whereas $\Delta E_{\text{int}}^{\text{hBN/hBN}}$ grows steadily (Fig. 4(d)). The critical role of ripple suppression is validated by constrained

simulations in which GNR out-of-plane motion is prohibited; under this condition, friction increases monotonically with N (Fig. S28 in the ESM). Thus, the friction minimum at $N \approx 16$ marks the point where the reduction from ripple suppression is balanced by the increase from cumulative h-BN/h-BN perturbations.

The modulation of dynamic friction can be further clarified by examining how different energy dissipation channels evolve with the number of encapsulating h-BN layers (N). Figures 5(a) and 5(c) show that the total steady-state dissipation power ($\langle P \rangle$) shows the same nonmonotonic dependence on N as the friction force (Fig. S29 in the ESM). The dissipation is found to be dominated by the vertical component (red curves in Figs. 5(a) and 5(c), consistent with prior observations in periodic graphene/h-BN heterostructures [96], where the competition between moiré ridge suppression and narrowing under pressure led to similar load-dependent frictional trends. In our encapsulated GNR system, however, the underlying mechanism differs. Statistical analysis of the atomic dissipation for the 6, 16, and 50 h-BN layers (Figs. 5(b) and 5(d) and Figs. S30 and S31 in the ESM) shows that it follows a lognormal distribution function:

$$\rho(x) = \frac{A}{x\sigma\sqrt{2\pi}} \exp\left(-\frac{(\ln x - \mu)^2}{2\sigma^2}\right) \quad (6)$$

where $x = \langle p_{\text{diss}}^j \rangle$, and A is an amplitude factor that scales the probability density function to match the histogram counts. μ and σ are the mean and the standard deviation of the distribution,

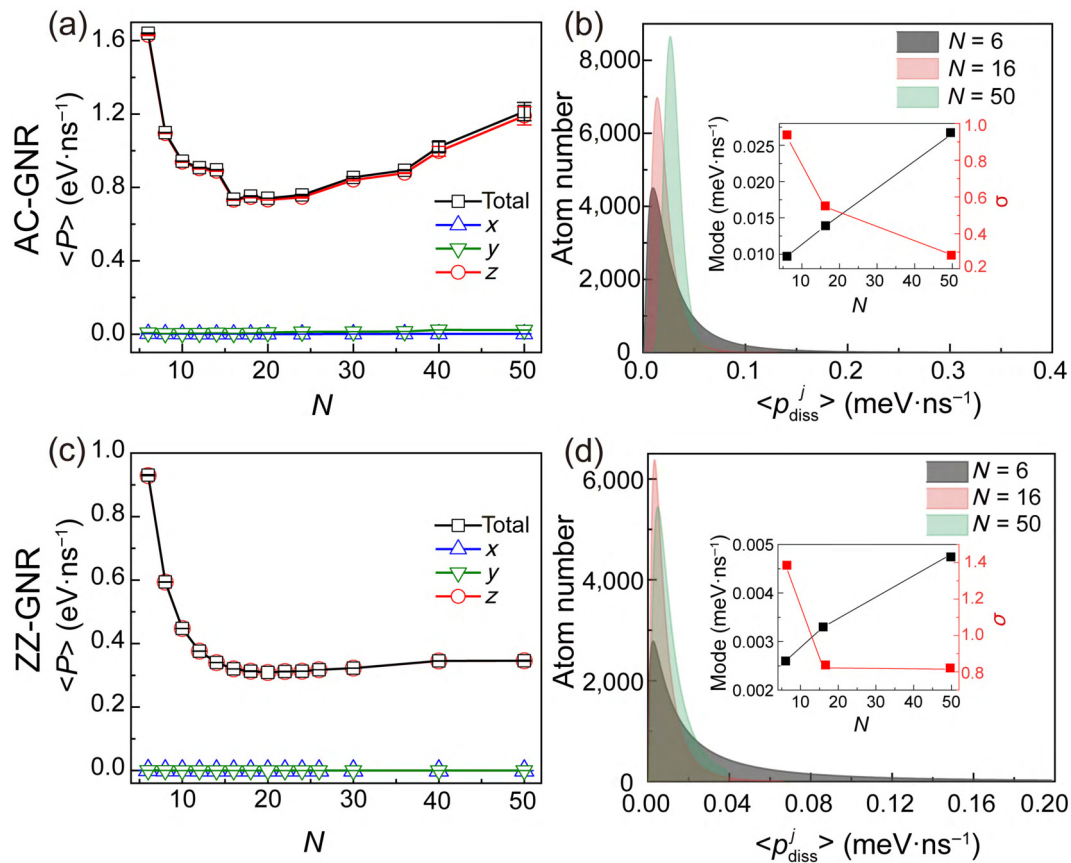


Fig. 5 Energy dissipation characteristics of embedded GNR systems as a function of the number of h-BN encapsulation layers. (a, c) Total steady-state dissipation power ($\langle P \rangle$) and its directional components as a function of the number of h-BN layers. (b, d) Lognormal fits of static distributions of atomic energy dissipation power ($\langle p_{\text{diss}}^j \rangle$) for embedded GNR systems with 6, 16, and 50 h-BN layers. The insets in (b, d) show the evolution of the mode ($e^{\mu-\sigma^2}$) and the standard deviation (σ). (a, b) correspond to embedded AC-GNR systems, while (c, d) correspond to embedded ZZ-GNR systems.

respectively. The mode ($e^{\mu-\sigma^2}$) extracted from the distribution provides the most likely dissipation value.

The detailed fitting parameters are summarized in Table S2 in the ESM. As the number of encapsulating h-BN layers (N) increases, the dissipation distribution evolves in two key ways (Figs. 5(b) and 5(d) and Fig. S32 in the ESM). First, the high-dissipation tail is gradually suppressed, eliminating rare but extreme energy loss events. Second, the mode ($e^{\mu-\sigma^2}$) shifts upward, indicating that the baseline level of atomic dissipation becomes higher. These two opposing trends give rise to the observed valley-shaped dependence of friction on encapsulation thickness: Friction decreases at intermediate N due to the suppression of extreme events but increases again at large N as the elevated baseline dissipation begins to dominate. This evolution is closely tied to the out-of-plane dynamics of the GNR. At low confinement, the pronounced ripples trigger intermittent high-dissipation bursts (Movie S3 in the ESM). Thicker encapsulation clamps these ripples (Fig. S26 in the ESM), reducing dissipation. At very high N , however, the ribbon exhibits a rapid oscillatory out-of-plane fluctuation mode during sliding (Movie S4 in the ESM), which shifts the baseline dissipation upward and results in the eventual friction increase.

4 Conclusions

In summary, our MD simulations reveal that GNRs embedded within AA'-stacked h-BN layers exhibit friction more than an order of magnitude lower than their on-surface counterparts, with sublinear length scaling that persists without saturation up to

hundreds of nanometers. The origin of this ultralow friction lies in registry competition at the encapsulated interfaces, which suppresses strain accumulation and stress localization, thereby enabling smooth collective sliding instead of soliton-mediated stick-slip. The friction can be further tuned by varying the encapsulation thickness, displaying a non-monotonic trend where a minimum occurs once the friction-reducing effect of pressure-induced ripple suppression balances the friction-increasing effect of cumulative h-BN/h-BN interlayer perturbations. These results clarify the microscopic origins of superlubricity in encapsulated vdW heterostructures and establish encapsulation as a practical approach for friction control. Beyond fundamental insight, this work offers guiding principles for designing robust, durable, and energy-efficient GNR-based nanoelectronic devices and scalable superlubric systems.

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Author contributions

Wengen Ouyang conceived and supervised the project. Sen Wang

designed and performed the simulations. Both authors analyzed the data, interpreted the results, and wrote the manuscript.

Availability of data and materials

The data that support the findings of this study are available from the corresponding author upon reasonable request.

Competing interests

The authors have no competing interests to declare that are relevant to the content of this article.

Electronic Supplementary Material

Supplementary material (spring stiffness sensitivity test; optimized model of GNR/h-BN systems; periodicity of the lateral force traces; chirality-dependent friction mechanism of embedded GNRs; sliding velocity sensitivity test; temperature sensitivity test; robustness of ultralow friction and sublinear friction-length scaling against width and chiral geometry; definition of the axial GNR unit cell; stress, strain, bond-length, registry, and displacement evolution of on-surface and embedded GNRs; effect of interlayer interaction on friction differences; stress evolution for short on-surface; energy dissipation analysis and its morphological origins; encapsulation pressure in embedded GNR system; effect of h-BN thickness on friction coefficients and dynamics of embedded GNR; statistical analysis of energy dissipation of embedded GNRs; stress evolution of embedded GNRs during sliding (Movie S1); stress evolution of on-surface GNRs during sliding (Movie S2); out-of-plane fluctuation of embedded GNRs encapsulated by six h-BN layers (Movie S3); out-of-plane fluctuation of embedded GNRs encapsulated by fifty h-BN layers (Movie S4)) is available in the online version of this article at <https://doi.org/10.26599/FRICT.2026.9441242>.

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