**Review** 

# Multi-scale synergic optimization strategy for dielectric energy storage ceramics

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**Abstract:** Dielectric capacitors, serving as the indispensable components in advanced high-power energy storage devices, have attracted ever-increasing attention with the rapid development of science and technology. Among various dielectric capacitors, ceramic capacitors with perovskite structures show unique advantages in actual application, e.g., excellent adaptability in high-temperature environments. And the optimization of their energy storage performance has become a hot research topic recently. This review presents the basic principles of energy storage in dielectric ceramics and introduces multi-scale synergic optimization strategies according to the key factors for superior energy storage performance. By summarizing the common points in numerous works, several universal modification strategies are reviewed, and future research on fatigue fracture of ceramic capacitors under multi-field including but not limited to force, electric, and thermal coupling conditions is also anticipated.

Keywords: dielectric capacitors; high-power; energy storage; multi-scale

# 1 Introduction

With the rapid development of economy and technology,

the demand for energy is continually increasing. However, the over-exploitation of traditional fossil resources such as oil and coal has caused a series of problems such as resource depletion and environmental degradation. In accordance with The Paris Agreement, the global carbon neutrality targets will be achieved by 2030, and total carbon dioxide emissions will be reduced by ~45% [1,2]. Therefore, it is very urgent to develop the new clean energy sources



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(such as solar, wind, and geothermal). Although the development of renewable energy is encouraged in recent years, it is still limited by many barriers such as intermittent and geographical limitations. In order to get rid of the dependence on fossil fuels, it is necessary to study energy storage and conversion devices. There are mainly three kinds of electrical energy storage devices: batteries, electrochemical capacitors, and dielectric capacitors [2-5]. Compared with batteries and electrochemical capacitors, dielectric capacitors do not involve any chemical reaction during the energy storage and release, so the discharge speed is extremely fast. Figure 1(a) shows the characteristics of these energy storage devices. It is clear that dielectric capacitors reveal distinctive features of ultra-high power density  $(10^6 - 10^7 \text{ W/kg})$  and fast charge/discharge rate (microsecond or even nanosecond) [6-9]. Therefore, they are widely utilized in high-power and high-pulse fields, such as electric vehicles, power grids, aircraft, and radar (Fig. 1(b)). In addition, they possess the advantages of simple preparation, no liquid component, high working voltage, a wide range of temperatures, good safety performance, etc. [10,11].

The research on dielectric capacitor materials has been a hot topic recently. The current mainstream research directions are divided into three categories: polymer dielectrics, film capacitors, and ceramic counterparts. Due to the low dielectric constants of polymer dielectrics, the energy density is badly limited. For example, the dielectric constant of biaxially oriented polypropylene (BOPP) is around 2.2, and the corresponding capacitors usually exhibit the small energy no more than 5 J/cm<sup>3</sup> [11,12]. The film capacitors

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generally show ultra-high energy density, but the total energy is quite low because of the limited volume [13,14]. Ceramic capacitors usually have high relative dielectric constant ( $\varepsilon_r$ ) up to 10<sup>3</sup>. For example, the  $\varepsilon_r$  of BaTiO<sub>3</sub> (BT)-based X7R-type ceramics can reach as high as 2000 [2,15]. Ceramic capacitors with large dielectric constants display great potential for energy storage performance. However, the limited breakdown

strength hinders their further increment of energy density. Therefore, stabilizing the dielectric constant while improving the electric breakdown strength  $(E_b)$  is of great importance for the ceramic capacitors.

In the present review, we introduce the principles of energy storage performance of ceramic capacitors, including the characteristics and influencing factors. Next, we list the current general strategies and methods to optimize the energy storage performance of ceramic capacitors. Finally, we summarize the optimal strategy for ceramic capacitors with high performance and look forward to the future development of ceramic capacitors.

# 2 Principle of energy storage of capacitors

#### 2.1 Energy storage and release

The energy storage of dielectric capacitor is based on the polarization (P) of internal dipoles upon applying the external electric field. Energy is stored and released in the process of polarization and depolarization, as shown in Fig. 2(a) [16,17]. Since no redox reaction or material transfer occurs during the whole process, the accumulated energy during charging process can be released quickly, generating a strong electrical pulse



**Fig. 1** (a) Comparison of power density and energy density capabilities of dielectric capacitors, electrochemical capacitors, and batteries [9]. (b) Applications for dielectric capacitors [2,11,25].



Fig. 2 (a) Circuit diagram of parallel plate dielectric capacitor. (b) Recoverable energy density ( $W_{rec}$ ) and energy storage loss ( $W_{loss}$ ) [17].

[11,16]. The energy stored per unit volume (i.e., charged energy density  $(W_{st})$ ) is expressed by Eq. (1):

$$W_{\rm st} = \frac{W}{Ad} = \frac{\int_0^{Q_{\rm max}} V \mathrm{d}Q}{Ad} = \int_0^{D_{\rm max}} E \mathrm{d}D \tag{1}$$

where A is the electrode area of capacitor, d is the thickness, W is the total energy stored in the dielectric capacitor, and V, Q,  $Q_{max}$ , E, D, and  $D_{max}$  represent the applied voltage, accumulated charge, maximum accumulated charge, applied electric field, electric displacement, and maximum electric displacement, respectively [8].

The *D* in dielectric materials is closely related to the polarization ( $D = P + \varepsilon_0 E$ ), while for high dielectric constant materials, *D* is approximately equal to  $P = \varepsilon_0 \varepsilon_r E$  ( $\varepsilon_0$  is the vacuum dielectric constant). For linear dielectric (LD) materials, the dielectric constant does not vary with the applied electric field, and  $W_{st}$  can be expressed by Eq. (2):

$$W_{\rm st} = \int_0^{D_{\rm max}} E \mathrm{d}D = \frac{1}{2} \varepsilon_0 \varepsilon_{\rm r} E^2 \tag{2}$$

For nonlinear dielectric materials, certain energy dissipation is exhibited during the charging and discharging due to the polarization hysteresis.  $W_{st}$  and  $W_{rec}$  can be obtained by integrating the integral area of the hysteresis line separately, as shown in Fig. 2(b) [18–20].

$$W_{\rm st} = \int_0^{P_{\rm max}} E dP \tag{3}$$

$$W_{\rm rec} = \int_{P_{\rm r}}^{P_{\rm max}} E dP \tag{4}$$

$$W_{\rm st} = W_{\rm rec} + W_{\rm loss} \tag{5}$$

$$\eta = \frac{W_{\rm rec}}{W_{\rm st}} \times 100\% \tag{6}$$

where  $P_{\text{max}}$  and  $P_{\text{r}}$  denote the maximum polarization and the residual polarization, respectively, and  $\eta$  is the energy efficiency. For dielectric materials, the main parameters to evaluate the energy storage capacity include  $W_{\text{rec}}$  and  $\eta$ . Therefore, it can be seen from Eq. (4) that dielectric materials with high  $P_{\text{max}}$ , low  $P_{\text{r}}$ , and high  $E_{\text{b}}$  are more valuable for applications of energy storage.

The  $E_{\rm b}$  of ceramic capacitors is affected by a variety of factors, including but not limited to relative density, ceramic thickness, grain size, resistivity, type of test voltage, and temperature [21-24]. It is found that the  $E_{\rm b}$  of ceramic capacitors can be improved by more than several times by reducing the thickness of ceramics because of the reduction in the probability of defects [23,25,26]. Moreover, a second phase cladding layer with low dielectric constants on ceramic grains is also effective to enhance  $E_b$  [21,27,28]. In addition, adjusting the fabrication process to decrease the grain size, modifying the ceramics to reduce the ionic conductivity, and boosting band gap  $(E_g)$  to prevent the electronic transition are of great significance to improve  $E_b$  of ceramic capacitors [27-29]. As the polarization modulation,  $P_{\text{max}}$  is related to the material features and vacancies, while  $P_{\rm r}$  can be optimized by resizing the domains [30–35].

## 2.2 Dielectric materials for energy storage capacitors

Dielectric materials for energy storage capacitors are usually classified into different categories according to their hysteresis loops, namely LDs, ferroelectrics (FEs), relaxor ferroelectrics (RFEs), and antiferroelectrics (AFEs). The related polarization–specific electric field behavior (i.e., P-E loop) and domain structures are shown in Fig. 3 [2,8,25].

Theoretically, the dielectric constant of LDs does not vary with the electric field, and thus exhibits the near-linear characteristic, as shown in Fig. 3(a). These materials are usually characterized by high  $E_{\rm b}$ , low dielectric loss, and low  $P_{\rm max}$ . The widely studied LD materials include TiO<sub>2</sub>, CaTiO<sub>3</sub>, and SrTiO<sub>3</sub> (ST) [36–38].

FEs normally reveal large  $P_{\text{max}}$  and high dielectric constants [39]. When the electric field is applied, the FE domains respond to the electric field, while the FE domains partly go back to their original states upon removing the electric field. Figure 3(b) displays the typical hysteresis *P*–*E* loops of FEs. The energy storage density of FEs is low due to the large  $P_{\rm r}$ . Therefore, they usually serve as the fillers to the glass- or polymermatrix to enhance the dielectric constants [40–43].





Fig. 3 Typical P-E loops of (a) LDs, (b) FEs, (c) RFEs, (d) AFEs, and (e) RAFEs [2,11].

Different from the FEs with long-range FE orders, the RFEs generally exhibit short-ranged FE orders with high  $P_{\text{max}}$ , low  $P_{\text{r}}$ , high dielectric constants, and slim P-E curves, as shown in Fig. 3(c). These features do favor to the excellent energy storage performance [44]. After the RFE was first discovered in the BT–BaSnO<sub>3</sub> system in 1954, most research focuses on Pb-based systems and lead-free Bi-based systems [45].

In AFEs, dipoles tend to arrange in pairs in the opposite directions, and therefore do not show polarity macroscopically [45,46]. When they are subjected to an external electric field, the AFE–FE phase transition will occur and give rise to a jump in polarization. When the applied electric field is switched off, it will revert from FE to AFE again. The P-E curve exhibits the characteristics of a double hysteresis loop, as shown in Fig. 3(d). The present research of AFE materials are mainly concentrated on the systems of (Pb,La)(Zr,Ti)O<sub>3</sub>, AgNbO<sub>3</sub> (AN), NaNbO<sub>3</sub> (NN), (Bi,Na)TiO<sub>3</sub> (BNT), etc. [34,47–51].

RAFEs are normally regarded as a special kind of AFE materials. Due to the disturbance of macro AFE orders and emergence of nanodomains with weak couplings, they usually tend to exhibit *P*–*E* curves with suppressed hysteresis, which is very different from typical AFEs. Thus, RAFEs show great potential in energy storage with the synergistic optimization of  $W_{\text{rec}}$  and  $\eta$ . The present research on RAFEs is mainly focused on AN-, BNT-, and NN-based systems [52–54].

Although dielectric materials have their advantages

in terms of energy storage, the energy density of ceramic materials is generally no more than 2 J/cm<sup>3</sup> due to limited dielectric constant, low  $E_b$ , or high dielectric loss [38,55,56]. The dielectric capacitors with high  $W_{rec}$  and energy efficiency should not only possess high dielectric constants and high  $E_b$ , but also require low dielectric loss and fast dielectric response, which are the main stream of present optimization of dielectric capacitors. Selecting appropriate ceramic materials and optimization methods is the key to improving the energy storage performance of dielectric capacitors.

# 3 Improvement strategies for energy storage performance

The ceramic capacitor is an energy storage device with a multi-scale structure, which exhibits different characteristics at different scales, as shown in Fig. 4. So, there are many methods to optimize the energy storage performance [57–59].

At the nanoscale, doping is often used to improve the intrinsic  $E_g$ , reduce the ion mobility, or enhance the conductive activation energy ( $E_a$ ), which is of great significance for large voltage tolerance [47,60–62]. Furthermore, doping can also affect phase structures and domain structures, which is an indispensable modification method for phase engineering and domain engineering [32,52,54,63–65].



Fig. 4 Structures and optimization strategies of ceramic capacitors at different scales.

At the microscale, constructing the core–shell structure and composite structure are two of the important ways to enhance the energy storage performance of ceramic capacitors [27,28,66–70]. For example, the dielectrics with a high  $E_b$  (e.g., SiO<sub>2</sub>) can be deposited on the surface of the FE materials with high polarization, which would enhance the apparent  $E_b$  of dielectric materials while retaining the high polarization [28,71]. The addition of insulating metallic oxide (such as ZnO, MgO, and Al<sub>2</sub>O<sub>3</sub>) will precipitate at the grain boundary to prevent ceramic broken down, and then enhance their  $E_b$  values [69,70,72].

At the mesoscale, reducing the grain size to improve the  $E_b$  is one of the most common modified methods. On the one hand, the reduction of the grain size increases the content of grain boundaries with high resistivity, which improves the dielectric breakdown resistance. On the other hand, the breakdown path of the electrical tree is more complex in fine-grained ceramics, and dielectric breakdown requires higher energy [22,73–75].

At the macroscale, the tape-casting and rolling process are two effective methods. The bulk ceramics prepared via the traditional solid-state reaction usually contain many defects and reveal low relative density, resulting in low  $E_b$  [76]. Multilayer ceramic capacitors (MLCCs) prepared via the tape-casting process can simultaneously increase the relative density and reduce the thickness of single-layer ceramics to greatly enhance  $E_b$ . The multilayer stacking also enables the miniaturization and integration of ceramic capacitors [23,34,57,58]. The rolling process involves pouring the mixture of ceramic powders and polyvinyl alcohol (PVA) into a roller, which is extruded and shaped to obtain high-density ceramics. The whole preparation

process is simple and suitable for industrial production [77,78].

It is reported that more than two modification strategies are often used together to enhance the energy storage performance. The modification methods at different scales have their own characteristics, and multi-scale collaborative optimization can improve the all-around performance of capacitors.

### 3.1 Nanoscale modification

The materials with perovskite structures (ABO<sub>3</sub>) for dielectric energy storage are the most widely investigated. The doping elements can be divided into A- and/or B-site doping according to the occupied position [34,63,79,80]. First, the ionic radius should be well chosen. On the one hand, the ionic radius of doping elements should be different from that of the element in the corresponding position to induce lattice distortions; on the other hand, too large radius differences between doping and host elements would result in the failure of doping. Second, the ionic valence states of them do not differ too much to avoid charge imbalance. Third, the substituted element cannot react with the A-/B-site elements to form the second phase or impurity. Doping is an effective mean of ceramic modification via phase engineering [33,52,81–83], domain engineering [32,64], and manipulating breakdown and polarization [47,61,62,84,85].

## 3.1.1 Phase engineering

Dielectric ceramics have abundant phase transitions. In some cases, the room-temperature phase structure is not conducive to energy storage [33,52]. Therefore, the construction of target phase regions via doping is a



valid and effective modification method to optimize the energy storage performance.

Lead-based AFE ceramics are widely used in the field of high power/pulses due to their excellent  $W_{rec}$  and  $\eta$ . The current research hotspots mainly include Pb(Zr,Ti)O<sub>3</sub> (PZT) [86], (Pb,La)(Zr,Ti)O<sub>3</sub> [81,87–89], (Pb,La)(Zr,Sn,Ti)O<sub>3</sub> [90–93], and (Pb,La)(Zr,Sn)O<sub>3</sub> [48,94].

PZT is a binary solid solution of PbZrO<sub>3</sub> (PZO) and PbTiO<sub>3</sub>. As shown in Fig. 5(a), PZT ceramics exhibit antiferroelectricity when the doping content of  $Ti^{4+}$  is within 0–5 mol% [86]. Interestingly, when  $La^{3+}$  and Sn<sup>4+</sup> are introduced, the doping content of  $Ti^{4+}$  can be increased from 5 to 10 mol% (Fig. 5(b)). In other words, the AFE phase region is expanded, providing more possibilities for the design of lead-based AFE materials [82,83].

PZT-based AFE ceramics have great potential for energy storage applications, but its energy efficiency is very limited due to large hysteresis induced by the phase transition [56]. A relaxation behavior is successfully constructed near the phase boundary by doping  $La^{3+}$  (Fig. 5(c)), which effectively disrupts the long-range AFE orders, generates polar nanoclusters,

Cubic

Rhombo eight <111

(a)

Temperature (°C)

400

300

20

10

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and finally exhibits elongated electrical hysteresis curves (Fig. 5(d)). Moreover,  $La^{3+}$  can also stabilize the AFE phase near the AFE-FE grain boundary [81,95–98]. The energy density of 3.04 J/cm<sup>3</sup> with an energy efficiency of 92% is realized in PLZT ceramics [81]. Due to the improved energy efficiency, the energy consumed in the form of heat during the cycling process is obviously reduced. The reliability is thus improved, and the performance remains unchanged after 10,000 cycles [81]. Zhang et al. [95] reported that the room-temperature phase changes from orthogonal AFE (AFE<sub>0</sub>) to tetragonal AFE (AFE<sub>T</sub>) after introducing  $\text{Sr}^{2+}$  into the (Pb<sub>0.97</sub>La<sub>0.02</sub>)(Zr<sub>0.75</sub>Sn<sub>0.195</sub>Ti<sub>0.055</sub>)O<sub>3</sub> system. Meanwhile, the stability of the AFE phase increases simultaneously. The energy density increases from 3.53 to 5.56 J/cm<sup>3</sup> as the doping content goes up to 1.5 mol%. Benefiting from the expansion of temperature region of the AFE phase, the energy density varies less than 12% in the temperature range of 30–90 °C [56,95].

Pb-based ceramics display a variety of phase regions, and thus reveal many possibilities to improve the energy storage capacity by adjusting the phase structure. Taking the  $(Pb_{1-1.5x}La_x)(Zr_{0.66}Sn_{0.23}Ti_{0.11})O_3$  (PLZST)



**(b)** 

Tetragonal

six <001>

Fig. 5 Phase diagrams of (a) PZO–Pb1rO<sub>3</sub> and (b)  $(Pb_{0.97}La_{0.02})(Zr,Sn,11)O_3$ . (c) Phase diagram and (d) energy storage performance of  $(Pb_{0.88}La_{0.08})(Zr_{0.91}Ti_{0.09})O_3$  (PLZT). Reproduced with permission from Ref. [86] for (a), © Springer Nature 2007; Ref. [82] for (b), © WILEY-VCH Verlag GmbH & Co. KGaA, Weinheim 2018; Ref. [81] for (c, d), © AIP Publishing LLC 2016.

ceramics for instance, when the content of  $La^{3+}$  exceeds 2 mol%, PLZST ceramic systems undergo an FE–AFE phase transition. As the content of  $La^{3+}$  is increased to 4 mol%, the energy density changes from ~0.1 to ~1.47 J/cm<sup>3</sup> in PLZST ceramics [99]. In addition to the  $La^{3+}$  content, the phase structure of PLZST ceramics can also be manipulated by changing the ratios of Zr, Sn, and Ti, as shown in Table 1.

The phase engineering of lead-free systems can be also efficiently designed and modulated via the atomic doping. AN is an AFE material with perovskite structures. Fu et al. [55] reported that AN undergoes an AFE-FE phase transition when the applied electric field exceeds 180 kV/cm and produces a large  $P_{\text{max}}$  of  $\sim$ 52  $\mu$ C/cm<sup>2</sup>, as shown in Fig. 6(a). At room temperature (RT), AN is the ferrielectric M<sub>1</sub> phase and exhibits ferrielectric properties that are not favorable for energy storage [102,103]. As the temperature rises, the phase structure gradually transforms into disordered AFE M<sub>2</sub> and M<sub>3</sub> phases, as shown in Fig. 6(b). Zhao et al. [34] found that the replacement of Nb<sup>5+</sup> by Ta<sup>5+</sup> with lower polarizability enhances the antiferroelectricity of AN, so that the disordered AFE M<sub>2</sub> phase can be successfully stabilized at RT (Fig. 6(c)). When the content of Ta<sup>5+</sup> is 15 mol%, the energy density and energy efficiency can be enhanced to  $\sim 4.2 \text{ J/cm}^3$  and  $\sim 69\%$ , respectively (Figs. 6(d) and 6(e)).

Since  $Ta^{5+}$  (0.64 Å, coordination number (CN) = 6) and Nb<sup>5+</sup> (0.64 Å, CN = 6) have the same ionic radius and valence state, AN and AgTaO<sub>3</sub> (AT) have the infinite miscibility [104]. Luo *et al.* [52] successfully implemented the design of relaxor AFE at the M<sub>2</sub>–M<sub>3</sub> phase boundary by adjusting the ratio of Nb to Ta in the AN–AT solid solution. As the Ta<sup>5+</sup> content increases, the M<sub>2</sub>–M<sub>3</sub> phase boundary is gradually stabilized at RT. Meanwhile, the *P–E* loops become slanted and slim. The obtained 0.45AN–0.55AT ceramics show the further enhanced  $W_{\rm rec}$  of 6.3 J/cm<sup>3</sup> and  $\eta$  of 90% at 470 kV/cm.

The phase structure modulation of AN can be also achieved by introducing A-site doping, such as  $La^{3+}$ ,  $Sm^{3+}$ ,  $Nd^{3+}$ ,  $Gd^{3+}$ , and  $Sr^{2+}$  [65,105–108]. The substitution of  $La^{3+}$  (1.36 Å, CN = 12) with a smaller ionic radius than  $Ag^+$  (1.48 Å, CN = 12) in the A-site of AN leads to lattice shrinkage, reduction in the lattice distortion, and enhancement in symmetry. The increment in the AFE phase stability is thus obtained [52,109]. The room-temperature phase structure of AN gradually changes from the FE M<sub>1</sub> phase to the AFE

Table 1Energy storage performance of PLZSTceramics with different ratios of Zr, Sn, and Ti

Composition	$E_{\rm b}$ (kV/cm)	$W_{\rm rec} ({\rm J/cm^3})$	η (%)	Ref.
$Pb_{0.97}La_{0.02}(Zr_{0.58}Sn_{0.35}Ti_{0.07})O_3$	118	2.35	86.1	[100]
$Pb_{0.97}La_{0.02}(Zr_{0.50}Sn_{0.46}Ti_{0.04})O_3$	150	3.2	86.5	[93]
$Pb_{0.97}La_{0.02}(Zr_{0.56}Sn_{0.35}Ti_{0.09})O_3$	175	3.3	80	[101]
$Pb_{0.97}La_{0.02}(Zr_{0.60}Sn_{0.35}Ti_{0.05})O_3$	200	4.1	_	[92]
$Pb_{0.97}La_{0.02}(Zr_{0.5}Sn_{0.44}Ti_{0.06})O_3$	250	4.2	82	[91]
$Pb_{0.97}La_{0.02}(Zr_{0.5}Sn_{0.45}Ti_{0.05})O_3$	400	5.6	63	[90]



**Fig. 6** (a) D-E and strain–E loops of AN ceramics, where f is the frequency. (b) Temperature (T) and  $\varepsilon_r$  dependence of dielectric constants of AN ceramics. (c) Phase diagram of AgNb<sub>1-x</sub>Ta<sub>x</sub>O<sub>3</sub> ceramics. (d) P-E loops of AN and AgNb<sub>0.85</sub>Ta<sub>0.15</sub>O<sub>3</sub> (ANT) ceramics. (e) Energy storage performance of AgNb<sub>1-x</sub>Ta<sub>x</sub>O<sub>3</sub> ceramics. Reproduced with permission from Ref. [55] for (a),  $\mathbb{C}$  American Institute of Physics 2007; Ref. [34] for (b–e),  $\mathbb{C}$  WILEY-VCH Verlag GmbH & Co. KGaA, Weinheim 2017.



 $M_2$  phase after the doping of  $La^{3+}$  for  $Ag^+$  [105]. The AFE feature is more pronouncedly demonstrated by the enhanced electric field of AFE-FE/FE-AFE phase transition  $(E_A/E_F)$ . As a result, the energy density reaches 3.12 J/cm<sup>3</sup> at 230 kV/cm in Ag<sub>0.94</sub>La<sub>0.02</sub>NbO<sub>3</sub> ceramics. Based on the same mechanism, Sm<sup>3+</sup> (1.24 Å, CN = 12) with a much smaller ionic radius than  $La^{3+}$  is also introduced to AN to replace Ag<sup>+</sup>. It is found that Sm<sup>3+</sup> has a more intense effect on the AN phase structure at RT, which completely transforms into the  $M_2$  phase with a higher energy density (> 3.5 J/cm<sup>3</sup>). With the optimized  $\text{Sm}^{3+}$  content of 3 mol%, the Ag<sub>0.91</sub>Sm<sub>0.03</sub>NbO<sub>3</sub> ceramics has an enhanced energy density up to 5.2 J/cm<sup>3</sup> at 290 kV/cm [65]. Moreover, Li et al. [107] and Mao et al. [110] also successfully achieved the construction of AN phase engineering by doping Gd<sup>3+</sup> and Lu<sup>3+</sup> with the energy densities of 4.5 and 3.5 J/cm<sup>3</sup>, respectively.

(K,Na)NbO<sub>3</sub> (KNN) is a binary solid solution of FE KNbO<sub>3</sub> and AFE NN. It possesses the strong FE characteristics with high  $P_{\text{max}}$  of ~50  $\mu$ C/cm<sup>2</sup> [111]. However, the application of KNN in energy storage is badly limited due to its low  $E_{\text{b}}$  and large hysteresis [112]. KNN exhibits a series of phase transitions of rhombohedral–orthorhombic–tetragonal–cubic (R–O–

T–C) with the rising temperature, as shown in Fig. 7(a). Chen *et al.* [33] introduced many special ions (Li<sup>+</sup>, Ba<sup>2+</sup>, Bi<sup>3+</sup>, Sc<sup>3+</sup>, Hf<sup>4+</sup>, Zr<sup>4+</sup>, Ta<sup>5+</sup>, and Sb<sup>5+</sup>) into the KNN ceramics to tailor  $T_{R-O}$ ,  $T_{O-T}$ ,  $T_{T-C}$ , and locally R–O–T–C multiphase nanoclusters (Fig. 7(b)). The R–O–T–C multiple phases can be directly observed in high-entropy KNN (KNN-H) ceramics by using atomic-resolution scanning transmission electron microscopy (STEM). The large number of polar nano-regions (PNRs) of ~1–3 nm can disrupt the long-range orders of the system, enhance the external electric field response rate of KNN-H ceramics, and thus improve the energy efficiency (Fig. 7(c)) [113]. A giant  $W_{rec}$  of ~10.06 J/cm<sup>3</sup> with ultra-high  $\eta$  of ~90.8% is successfully achieved in KNN-H ceramics (Fig. 7(d)).

In other lead-free systems, such as BiFO<sub>3</sub> (BF), BNT, and NN ceramics, the phase structure construction is also frequently used to improve the energy density and energy efficiency. For example,  $W_{\rm rec}$  of ~2.21 J/cm<sup>3</sup> and  $\eta$  of ~76% are realized in BF-based ceramics by constructing mixed phases of *R*3*c* rhombohedral and *Pbnm* orthorhombic phase [114,115]. Qi and Zuo [53] obtained a  $W_{\rm rec}$  of 7.02 J/cm<sup>3</sup> with  $\eta$  of 85% by introducing NN components into BNT ceramics to stabilize the AFE phase at RT.



**Fig.** 7 Dielectric performance of (a) KNN and (b) KNN-H ceramics. (c) P-E loops and (d) energy storage performance of KNN-H ceramics. Reproduced with permission from Ref. [33],  $\bigcirc$  The Author(s) 2022.

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#### 3.1.2 Domain engineering

High energy efficiency is one of the key indexes to evaluating the performance of ceramic capacitors. The low efficiency means large energy loss during the charge/discharge process. The energy loss of ceramic capacitors will be released in the form of thermal or mechanical energy, which will seriously deteriorate the electric breakdown of capacitors and limit their reliability in practice. The design of domain size and structures is very effective to enhance the energy efficiency. In ceramic materials, the nanodomains with weak couplings are very sensitive to the external electric field, so ceramic capacitors with a large number of nanodomains or PNRs tend to show slim *P–E* curves, accompanied by very small energy loss [29,32,47,64,116].

As AFE materials with the first order AFE–FE phase transition, AN is prone to showing large hysteresis during the transition process, which badly harms its energy storage efficiency [52]. Therefore, many research groups have spared no effort to construct nanodomains in AN ceramics to improve the energy efficiency. It is reported that the size of AFE domains can be reduced to less than 100 nm by substituting La<sup>3+</sup> for Ag<sup>+</sup> in AN ceramics [63]. The introduction of La<sup>3+</sup> interrupts the long-range AFE orders, gives rise to nanodomains, and finally enhances  $\eta$  [63]. As shown in Fig. 8(a), well-ordered lamellar AFE microdomains and a large domain wall density can be observed in



Fig. 8 (a) Dark-field TEM micrographs of ALN(x) ceramics along the orthorhombic [401] zone axis; the insets are the corresponding selected area electron diffraction patterns and the dark-field TEM image used the reflection that the arrows mark. (b–e) P-E and current density (I)–E loops of ALN(x) ceramics. Reproduced with permission from Ref. [63],  $\bigcirc$  Elsevier B.V. 2020.



Ag<sub>0.82</sub>La<sub>0.06</sub>NbO<sub>3</sub> (ALN(0.06)) ceramic grains [117]. With the increasing La<sup>3+</sup>, nano-sized AFE domains gradually appear, and the coexistence of micron and nano-sized AFE domains can be observed in ALN(0.08) ceramics. Nanodomains finally dominate with the further increment of La<sup>3+</sup> (ALN(0.10)). Together with the change in domain size, the variation of *P*–*E* curves also occurs (Figs. 8(b)–8(e)). Because the nanodomains respond rapidly to the external electric field, the *P*–*E* curves of ceramics with La<sup>3+</sup> doping appear to be more "slender" than those of pure AN ceramics. Moreover, La<sup>3+</sup> also stabilizes the AFE stability of ceramics. The  $W_{\text{rec}}$  and  $\eta$  are 7.01 J/cm<sup>3</sup> and 77% at 476 kV/cm in ALN(0.10) [63], respectively.

Utilizing Nd<sup>3+</sup> to replace Ag<sup>+</sup> on the A-site of AN ceramics can also reduce the domain sizes. The doping of Ag<sup>+</sup> by Nd<sup>3+</sup> produces Nd<sub>Ag</sub>, which disrupts the antipolar orders and leads to a decrement in domain size. The domain width decreases from ~1 to < 0.3 µm when the content of Nd<sup>3+</sup> increases to 3 mol%. The *P*–*E* curves change from square-shape with large hysteresis to the slim ones with low hysteresis after the co-doping of Nd<sup>3+</sup> and Ta<sup>5+</sup>. In addition, the introduction of Ta<sup>5+</sup> stabilizes the antiferroelectricity, so that the Ag<sub>0.97</sub>Nd<sub>0.01</sub>Ta<sub>0.20</sub>Nb<sub>0.80</sub>O<sub>3</sub> ceramics exhibit large phase transition electric fields and achieve the *W*<sub>rec</sub> of 6.5 J/cm<sup>3</sup> and  $\eta$  of 71% at 370 kV/cm. Similarly, Shi *et al.* [106] also observed AFE domains of 50–100 nm

size in 1% Nd-doped AN ceramics and obtained  $W_{\rm rec}$  of ~4.6 J/cm<sup>3</sup> and  $\eta$  of ~62.5%. Gao *et al.* [118] constructed AFE domains with a width of ~150 nm in Ag<sub>0.91</sub>Sm<sub>0.03</sub>NbO<sub>3</sub> ceramics and successfully upgraded  $W_{\rm rec}$  and  $\eta$  to 4.3 J/cm<sup>3</sup> and 66%, respectively. Beside the rare earth elements, Sr<sup>2+</sup> and Zn<sup>2+</sup> are also utilized to build nanodomains in AN ceramics [108,119].

BT is a typical FE material with strong spontaneous polarization. And the large  $P_r$  and hysteresis greatly limit the energy storage properties, especially for  $\eta$ . Therefore, the construction of PNRs is a common modification method to enhance the energy efficiency [28,32,64,66]. Yuan et al. [32] reported the transition of BT from normal FEs to highly diffused and dispersed RFEs after incorporating Bi(Mg<sub>0.5</sub>Zr<sub>0.5</sub>)O<sub>3</sub> (BMZ), accompanied by the generation of PNRs. As BMZ increases up to 5 mol%, the microstructures change from ordered lamellar domains (100 nm in width, Fig. 9(a)) to miniaturized lamellar domains (20-30 nm in width, Fig. 9(b)) surrounded by PNRs. With the further increment of BMZ, the FE domains gradually decrease, and PNRs gradually occupy the whole view (Fig. 9(c)). Since PNRs respond quickly to the applied electric field, the slim P-E loops with a suppressed hysteresis are obtained in Fig. 9(d). Finally, the  $W_{\rm rec}$  of 2.9 J/cm<sup>3</sup> and  $\eta$  of 86.8% are achieved in BT-BMZ ceramics (Fig. 9(e)).



**Fig. 9** Bright-field TEM micrographs of (1-x)BT-xBMZ ceramics for (a) x = 0, (b) x = 0.05, and (c) x = 0.15. (d) *P*–*E* loops and (e) energy storage performance of (1-x)BT-xBMZ ceramics. Reproduced with permission from Ref. [32], © Elsevier Ltd. 2018.



In 2021, Dai et al. [64] constructed PNRs in

(BCZT)  $Ba_{0.85}Ca_{0.15}Zr_{0.1}Ti_{0.9}O_3$ by introducing  $Bi(Mg_{2/3}Nb_{1/3})O_3$  (BMN), which can effectively alleviate the hysteresis and eventually facilitate the ultra-high  $\eta$  of ~90.5% and  $W_{\rm rec}$  of ~3.81 J/cm<sup>3</sup>. When the applied electric field is switched off, the wellordered FE domains cannot return to their initial states, which is the main reason for the low energy density and energy efficiency of BCZT ceramics. After the introduction of BMN, the long-range ordered structures are interrupted, and nanodomains appear. They can quickly return to the initial state upon the removing of applied electric field, which leads to low hysteresis and low  $P_{\rm r}$ . A large number of highly dynamic polar nanodomains were constructed in (Bi0.5Na0.5)0.65Sr0.35TiO3 (BNST) ceramics via introducing BMZ. The long-range ordered polarities and the early polarization saturation were efficiently suppressed. With the help of refined grains and compact structure, 0.9BNST-0.1BMZ ceramic revealed a high  $E_{\rm b}$  up to 522 kV/cm, the large  $W_{\rm rec}$  of 8.46 J/cm<sup>3</sup> and  $\eta$  of 85.9% [120].

# 3.1.3 Breakdown and polarization

In dielectric energy storage materials,  $E_b$  and polarization are usually a pair of contradictory properties. And most materials tend to have only one of them at the most [112]. How to resolve such paradox becomes the key to improve the energy storage performance.

1) *E*<sub>b</sub>

In general, the energy density of capacitors is related to the square of  $E_b$ , and thus  $E_b$  is an important parameter affecting the energy storage performance [121–124]. Factors affecting  $E_{\rm b}$  of ceramics include but are not limited to sample thickness, grain size, relative density, temperature, voltage type, and electrode shape/size [25]. According to the restrictive factors of  $E_{\rm b}$ , breakdown mechanisms are classified as intrinsic breakdown, electromechanical breakdown, thermal breakdown, partial discharge breakdown, etc. [25,121,122]. This subsection mainly focuses on how to enhance the intrinsic breakdown, which is the most widely investigated.

The  $E_g$  refers to the forbidden energy between the top of the valence band (VB) and the bottom of the conduction band (CB), which is usually closely related to the intrinsic dielectric breakdown [60].

$$E_{\rm b} = 1.36 \times 10^7 (E_{\rm g} / 4.0)^3 (\rm V / \rm cm)$$
 (7)

In general,  $E_g > 4.0$  eV is considered to be insulated, and 0.0 eV  $< E_g < 4.0$  eV and  $E_g = 0.0$  eV are regarded as semiconductors and metals, respectively. The  $E_g$  can be enhanced by forming the solid solution with enhanced resistivity, leading to the increment in  $E_b$ [125,126].

Figure 10(a) shows the  $E_g$  of various lead-free energy storage ceramics. The highest value of ~3.5 eV is found in NN ceramics [48,53,109,112,127–130]. Therefore, NN is often chosen as an additive to enhance the  $E_g$  of other dielectric ceramics. Qi *et al.* [24] studied the (0.67–*x*)BiFeO<sub>3</sub>–0.33BaTiO<sub>3</sub>–*x*NaNbO<sub>3</sub> (BF–BT–NN) ceramics, as shown in Fig. 10(b), where the  $E_g$  of BF-based ceramics monotonously increases with the NN content. The larger  $E_g$  means the more difficulty for electrons to jump from VB to CB, and thus larger  $E_b$  [60]. Finally,  $E_b$  is enhanced to 360 kV/cm at x = 0.1 (Fig. 10(c)). And  $W_{rec}$  and  $\eta$  achieve ~8.12 J/cm<sup>3</sup> and ~90%, respectively (Fig. 10(d)).

CaHfO<sub>3</sub> (CH) is a compound with ultra-large  $E_{g}$  of  $\sim$ 6.4 eV [61]. It is rational to utilize it as a modifier to optimize the  $E_{g}$ ,  $E_{b}$ , and energy storage performance of dielectric ceramics [61]. In the  $(1-x)Bi_{0.47}Na_{0.47}Ba_{0.06}TiO_3-xCaHfO_3$ (BNBT-CH) ceramics, the highest  $E_g$  of ~3.24 eV is obtained in 0.88BNBT-0.12CH ceramics (Fig. 11(a)) [62]. Meanwhile, the  $E_b$  is improved from 120 to 280 kV/cm (Fig. 11(b)), and  $W_{\rm rec}$  and  $\eta$  are elevated to 4.2 J/cm<sup>3</sup> and 66.7%, respectively (Fig. 11(c)), which are 711% and 138% of the BNBT without CH, respectively. Similarly, after adding Ca(Hf<sub>0.2</sub>Ti<sub>0.8</sub>)O<sub>3</sub> (CHT) to AN ceramics,  $E_{\rm g}$  increases from 2.72 to 2.80 eV (Fig. 11(d)), and  $E_b$  enhances from 200 to 325 kV/cm (Fig. 11(e)). The best comprehensive performance is obtained in 0.94AgNbO<sub>3</sub>-0.06Ca(Hf<sub>0.2</sub>Ti<sub>0.8</sub>)O<sub>3</sub> (AN-CHT0.06) ceramics with the  $W_{\rm rec}$  of ~5.4 J/cm<sup>3</sup> and  $\eta$  of ~66% (Fig. 11(f)) [61]. Dai et al. [131] optimized the energy storage performance via increasing the  $E_{g}$  to ~3.21 eV and reducing the grain size to  $\sim 0.21 \ \mu m$  in 0.825  $(K_{0.5}Na_{0.5})NbO_3-0.175Sr(Sc_{0.5}Nb_{0.5})O_3$  (0.825KNN-0.175SSN) ceramics, leading to a high  $E_{\rm b}$  of 395 kV/cm and  $W_{\rm rec}$  of 4.42 J/cm<sup>3</sup>.

2) Polarization

Bi(Me'Me")O<sub>3</sub> (Me' = Mg<sup>2+</sup> and Zn<sup>2+</sup>; Me" = Ti<sup>4+</sup> and Nb<sup>5+</sup>) are used to enhance the polarization of ceramics due to their unique configuration of lone pair electrons of Bi<sup>3+</sup> 6s, which is capable of hybridization with O<sup>2-</sup> 2p orbitals, leading to the high polarization of Bi-based ceramics [132–136]. At the same time, the introduction of Bi(Me'Me")O<sub>3</sub> facilitates forming PNRs, which are easier to align and switch back with the loading and unloading external electric





**Fig. 10** (a) Comparison of  $E_g$  values between different ceramics. (b) Variation of grain size ( $G_a$ ) and  $E_g$  of BF–BT–NN ceramics. (c) P-E loops and (d) energy storage performance of BF–BT–NN ceramics. Reproduced with permission from Ref. [116] for (a), © WILEY-VCH Verlag GmbH & Co. KGaA, Weinheim 2019; Ref. [24] for (b–d), © WILEY-VCH Verlag GmbH & Co. KGaA, Weinheim 2019.



**Fig. 11** (a) Ultraviolet–visible absorbance spectra and optical  $E_g$  of BNBT–CH ceramics. (b) P–E loops and (c) energy storage performance of BNBT–CH ceramics. (d) Schematic diagram of energy band structures of AN–CHT ceramics, where  $E_C$  and  $E_V$  are the energy of the CB and VB, respectively. (e) P–E loops and (f) energy storage performance of AN–CHTx ceramics. Reproduced with permission from Ref. [62] for (a–c),  $\bigcirc$  Elsevier B.V. 2021; Ref. [61] for (d–f),  $\bigcirc$  Elsevier B.V. 2021.

fields, and thus show small  $P_r$  in P-E loops [64]. In general, the  $P_{\text{max}}$  of dielectric ceramics generally decays with the increment of doping elements. However, the opposite phenomenon is observed in BT–Bi(Mg<sub>1/2</sub>Hf<sub>1/2</sub>)O<sub>3</sub> (BT–BMH) ceramics [84]. As shown in Figs. 12(a)–12(c), the  $P_{\text{max}}$  of BT–BMH ceramics increased slightly after doping [84], which is attributed to the orbital hybridization of  $\text{Bi}^{3^+}$  6s with  $O^{2^-}$  2p and the increased  $E_b$  simultaneously. With the synergic effect of enhanced  $P_{\text{max}}$ ,  $E_b$ , and suppressed  $P_r$ , the  $W_{\text{rec}}$  and  $\eta$  of BT-based ceramics go up to 3.38 J/cm<sup>3</sup> and 87% at 240 kV/cm, respectively (Fig. 12(d)). BMN is also introduced into 0.7Bi<sub>0.5</sub>Na<sub>0.5</sub>TiO<sub>3</sub>–0.3Sr<sub>0.7</sub>Bi<sub>0.2</sub>TiO<sub>3</sub> (BNT–SBT) ceramics to realize a small  $P_r$  of



~1.5  $\mu$ C/cm<sup>2</sup> and high  $P_{\text{max}}$  of ~48  $\mu$ C/cm<sup>2</sup>. A large  $P_{\text{max}} - P_{\text{r}}$  of ~46  $\mu$ C/cm<sup>2</sup> is achieved in BNT–SBT– BMN ceramics (Fig. 12(e)), leading to ultra-high  $W_{\text{rec}}$  of 7.5 J/cm<sup>3</sup> and  $\eta$  of 92% (Fig. 12(f)) [47]. In addition to BMH and BMN, many other Bi-based perovskite compounds are also demonstrated to be effective to enhance polarization, such as Bi(Ni<sub>2/3</sub>Nb<sub>1/3</sub>)O<sub>3</sub>, Bi(Mg<sub>0.5</sub>Ti<sub>0.5</sub>)O<sub>3</sub>, and BMZ, as shown in Table 2.

 $W^{6+}$  is also commonly used to enhance the polarization. After introducing  $W^{6+}$  into AN ceramics, a significant decrement in  $P_r$  and an increment in  $P_{max}$  are observed, which favor the energy density a lot (Figs. 13(a) and 13(b)) [142]. The doping of  $W^{6+}$  alleviates the oxygen vacancies, weakens the pinning effect, and thus enhances the polarization [30]. In addition,  $W^{6+}$  can also stabilize the antiferroelectricity and increase the critical phase transition electric fields.  $W_{\rm rec}$  of 3.3 J/cm<sup>3</sup> and  $\eta$  of 50% are finally obtained at 200 kV/cm (Fig. 13(c)).  $W^{6+}$  can also improve the ferroelectricity in PZO film [143].  $W^{6+}$  replacement of Zr<sup>4+</sup> gives rise to lattice distortion and ferroelectricity in PZO film, thus leading to higher polarization (Fig. 13(d)).



**Fig. 12** (a-c) *P*–*E* loops and (d) energy storage performance of BT–BMH ceramics. (e) *P*–*E* loops and (f) energy storage performance of BNT–SBT–BMN ceramics. Reproduced with permission from Ref. [84] for (a–d),  $\mathbb{O}$  Elsevier B.V. 2021; Ref. [47] for (e, f),  $\mathbb{O}$  Elsevier B.V. 2021.

Table 2	<b>Energy</b> storage	performance of	of ceramics	containing	Bi(Me'Me''	)0,
		P				/~ 3

Composition	$P_{\rm max}$ ( $\mu$ C/cm <sup>2</sup> )	$W_{\rm rec} (\rm J/cm^3)$	η (%)	$E_{\rm b}$ (kV/cm)	Ref.
0.88BT-0.12Bi(Ni <sub>2/3</sub> Nb <sub>1/3</sub> )O <sub>3</sub>	24.01	2.09	95.9	200	[137]
$0.88BT - 0.048Bi(Li_{0.5}Nb_{0.5})O_3 - 0.072Bi(Mg_{0.5}Ti_{0.5})O_3$	22.5	2.4	91.5	290	[138]
$0.85BT-0.15Bi(Mg_{0.5}Zr_{0.5})O_3$	23.2	2.9	86.8	300	[32]
$0.9BST-0.1Bi(Mg_{2/3}Nb_{1/3})O_3$	21.5	3.34	85.71	400	[139]
$0.925BCZT{}0.075Bi(Mg_{2/3}Nb_{1/3})O_3$	26.2	3.81	90.5	405	[64]
$0.6BT-0.4Bi(Mg_{1/2}Ti_{1/2})O_3$	42.2	4.49	93	340	[140]
$0.62NBT{-}0.3SBT{-}0.08Bi(Mg_{2/3}Nb_{1/3})O_3$	48	7.5	92	470	[47]
$0.97AN - 0.01Bi(Zn_{2/3}Nb_{1/3})O_3$	53.8	4.6	57.5	220	[119]
$0.35BF-0.65(0.85BT-0.15Bi(Sn_{0.5}Zn_{0.5})O_3)$	38.5	3.06	92	185	[141]





**Fig. 13** (a) P-E loops, (b)  $P_{\text{max}} - P_{\text{r}}$ , and (c) energy storage performance of W<sup>6+</sup>-doped AN ceramics. (d) P-E loops of W<sup>6+</sup>-doped PZO films. Reproduced with permission from Ref. [142] for (a–c), © American Chemical Society 2017; Ref. [143] for (d), © AIP Publishing LLC 2013.

Besides, there are other methods to enhance the polarization. For example, Nd<sup>3+</sup>-doped AN induces Nd<sup> $\pi$ </sup> and V'<sub>Ag</sub> at A-sites [31]. The polarization increases from ~43 to ~60 µC/cm<sup>2</sup>, which may be related to the increased concentration of silver vacancies [30]. Wang *et al.* [144] utilized an average ionic polarizability design strategy to enhance the *W*<sub>rec</sub> by sustaining high polarization and simultaneously improved  $\eta$  by disrupting the polar order in (1–*x*) (0.7BNT–0.3SBT)–*x*Sr(Zn<sub>1/3</sub>(Nb<sub>0.85</sub>Ta<sub>0.15</sub>)<sub>2/3</sub>)O<sub>3</sub> ceramics. The polarization was finally stabilized at > 41 µC/cm<sup>2</sup>, and the *W*<sub>rec</sub> and  $\eta$  were as high as 5.2 J/cm<sup>3</sup> and 91%, respectively.

In some cases, the introduction of doping elements can not only enhance the polarization but also reduce the ceramic grain size, leading to high  $P_{\text{max}}$  and  $E_{\text{b}}$ [27,30]. For example, Gao *et al.* [145] introduced Bi(Mg<sub>0.5</sub>Sn<sub>0.5</sub>)O<sub>3</sub> (BMS) into (Na<sub>0.5</sub>Bi<sub>0.5</sub>)<sub>0.65</sub>Sr<sub>0.35</sub>TiO<sub>3</sub> (NBST) ceramics. When the BMS content raises from 0 to 10 mol%, the ceramic grain size reduces from 4.17 to 0.67 µm, and the  $E_{\text{b}}$  enhances from 220 to 405 kV/cm. Moreover, due to the strong orbital hybridization of Bi<sup>3+</sup> 6s with O<sup>2-</sup> 2p, the  $P_{\text{max}}$  of NBST–BMS increases from ~46 to ~51 µC/cm<sup>2</sup>. Finally, the  $W_{\text{rec}}$  of 6.68 J/cm<sup>3</sup> and  $\eta$  of 89.1% are obtained [132,141]. Zhang *et al.* [146] prepared KNN-based ceramics with high  $P_{\text{max}}$  of ~48 µC/cm<sup>2</sup> and high  $E_{\text{b}}$  of ~330 kV/cm via introducing (K<sub>0.7</sub>Bi<sub>0.3</sub>)NbO<sub>3</sub>. The  $P_{\text{max}}$  and  $E_{\text{b}}$  are enhanced by 33% and 230%, respectively, over the undoped samples.

#### 3.2 Microscale modification

#### 3.2.1 Core-shell structure

It is reported that the shell, which is only a few nanometers thick near the grain boundaries, displays different compositions and properties from the core part [66]. The core–shell structure in ceramics is generally composed of FE, RFE, or non-FE (such as LD material and glass) [21]. For example, adding glass powders to FE ceramics is a common method to fill at the grain boundaries and enhance the  $E_b$  [147,148]. Similarly, combining the glass phase with (Pb<sub>0.97</sub>La<sub>0.02</sub>) (Zr<sub>0.56</sub>Sn<sub>0.35</sub>Ti<sub>0.09</sub>)O<sub>3</sub> ceramics can change the  $E_b$  from 110 to 150 kV/cm, while the energy density is increased to 3.3 J/cm<sup>3</sup> [101]. Wu *et al.* [149] constructed an "FE–paraelectric" core–shell structure via wrapping BT grains with ST, which simultaneously enhances the  $E_b$  and maintains high dielectric constants.

Recently, Yuan *et al.* [28] reported a unique bioinspired raspberry-like hierarchically structure of *x*wt%BT–BMZ/BaTiO<sub>3</sub>–Bi(Mg<sub>0.5</sub>Zr<sub>0.5</sub>)O<sub>3</sub>@SiO<sub>2</sub> (BBSx)

nanograins, as shown in Fig. 14(a). The experimental characterization and theoretical simulation confirm that the synergic effect of raspberry-like structure and insulating  $SiO_2$  nanocoating significantly improves the  $E_b$  and sustains large polarization of the nanocomposites [28,150].  $BaTiO_3$ -Bi(Mg<sub>0.5</sub>Zr<sub>0.5</sub>)O<sub>3</sub>@SiO<sub>2</sub>  $(BT-BMZ@SiO_2)$ fine powders with a grain size of ~50 nm are obtained via the high-energy ball milling and SiO<sub>2</sub> coating, followed by the mixing with BT-BMZ of ~500 nm to gain composites (Fig. 14(b)). The phase field simulations (Fig. 14(c)) reveal that the ceramics with 7 wt% nanofine powders exhibit the most complex breakdown path. Together with a large polarization guaranteed by the submicron BT-BMZ grains, BBS7 ceramics display a  $W_{\rm rec}$  of 3.14 cm<sup>3</sup> with  $\eta$  of 85.1%.

Jin *et al.* [66] prepared a kind of BaTiO<sub>3</sub>@(K,Na)NbO<sub>3</sub> (BT@KNN) ceramics, and the KNN shell was fabricated on BT grains of ~50 nm. Many nanodomain structures with sizes less than 100 nm can be observed, which is sensitive to the electric field response with low potential barriers. Moreover, the coexistence of the R-phase and the T-phase can be observed at the core position. Multiple nanodomain structures in BT@KNN ceramics are beneficial to low hysteresis and  $P_r$ , while the BT phase can maintain large  $P_{\text{max}}$ . Therefore, a large  $P_{\text{max}} - P_r$  of ~21.3 µC/cm<sup>2</sup> is obtained at 210 kV/cm, leading to  $W_{\text{rec}}$  of ~1.91 J/cm<sup>3</sup> and  $\eta$  of ~84.8%.

Core–shell structures can combine two materials with different properties to break the paradox between some parameters, such as polarization and  $E_b$ . By wrapping a layer of SiO<sub>2</sub> on the surface of AN,  $E_b$  is raised from 180 to 250 kV/cm, while  $P_{\text{max}}$  is stabilized at 34.5  $\mu$ C/cm<sup>2</sup> [21]. Based on this, Bi<sup>3+</sup> and Sc<sup>3+</sup> are introduced, and  $E_b$  is further increased to 322 kV/cm, while  $P_{\text{max}}$  is increased to 45  $\mu$ C/cm<sup>2</sup> [27]. Wang *et al.* [151] prepared BaTiO<sub>3</sub>@3% FeO (BT@FeO) ceramics with grain sizes of ~70 nm by coating the FeO layer on the surface of BT particles via the sol–gel method. The energy density and energy efficiency are 1.5 J/cm<sup>3</sup> and 88%, respectively, which are 500% and 175% higher compared to those of the uncoated one, respectively. Table 3 summarizes the energy storage performance of ceramics with core–shell structures.

## 3.2.2 0–3 type composite

According to the reported organic–inorganic composites, interfacial effects can significantly enhance the energy storage performance [8,158]. Similarly, the energy storage performance can also be optimized by designing 0–3 type composites in inorganic materials [69,70,72].

Recently, Li *et al.* [69] reported a novel 0–3 type (Bi<sub>0.32</sub>Sr<sub>0.42</sub>Na<sub>0.20</sub>)TiO<sub>3</sub>/MgO (BNST/MgO) composite with high  $E_b$ , as shown in Fig. 15(a). Compared with (Bi<sub>0.32</sub>Sr<sub>0.42</sub>Na<sub>0.20</sub>)TiO<sub>3</sub> ceramics with high  $\varepsilon_r$  of ~1900, the  $\varepsilon_r$  of MgO and MgTiO<sub>3</sub> are as low as 10 and 17, respectively (Fig. 15(b)). The results of the phase field simulations show that there existed a distortion of the electric potential and local electric field after the MgO/MgTiO<sub>3</sub> second phase with low  $\varepsilon_r$  is introduced



**Fig. 14** (a) Raspberry-like hierarchically structures of BBS*x* ceramics. (b) Representative bright-field TEM image of the BBS7 ceramics. (c) Breakdown paths of BBS*x* ceramics (x = 0, 7, and 100) simulated by the finite element method. Reproduced with permission from Ref. [28], © WILEY-VCH Verlag GmbH & Co. KGaA, Weinheim 2020.



Composition	Grain size (µm)	$E_{\rm b}$ (kV/cm)	$W_{\rm rec}$ (J/cm <sup>3</sup> )	η (%)	Ref.
BT-BMZ/BT-BMZ@SiO2	0.2	345	3.41	85.1	[28]
BT@NiO	1	230	2.72	70	[152]
BT@FeO	0.07	300	1.5	88	[151]
BT@KNN	0.194	211	2.24	84.8	[66]
BT@2 wt% SiO2	—	202	1.2	53.8	[71]
0.95(BT-BNT-Nb)-0.05BNT	—	230	1.91	91	[153]
Mn-AN@SiO2	2.72	244	3.34	60	[21]
Mn-AN@SiO <sub>2</sub> +Bi/Sc	2.2	322	5.9	71	[27]
$(BNT@La_{2}O_{3})-(SrSn_{0.2}Ti_{0.8}O_{3}@La_{2}O_{3})-Bi_{2}O_{3}-B_{2}O_{3}-SiO_{2}$	0.76	275	2.25	82.1	[154]
$0.96 (0.65BNT - 0.35Sr_{0.85}Bi_{0.1}TiO_3) - 0.04NN$	1.48	248	3.08	81.4	[155]
$Pb_{0.91}La_{0.06}(Zr_{0.552}Sn_{0.368}Ti_{0.08})O_3@PbO-B_2O_3-SiO_2-Al_2O_3-ZnO-MnO_2-Al_2O_3-ZnO-Al_2O_3-ZnO-Al_2O_3-ZnO-Al_2O_3-ZnO-Al_2O_3-ZnO-Al_2O_3-ZnO-Al_2O_3-ZnO-Al_2O_3-ZnO-Al_2O_3-ZnO-Al_2O_3-ZnO-Al_2O_3-ZnO-Al_2O_3-ZnO-Al_2O_3-ZO_3-ZnO-Al_2O_3-ZNO-Al_2O_3-ZNO-Al_2O_3-ZNO-Al_2O_3-ZNO-Al_2O_3-ZNO-Al_2O_3-ZNO-Al_2O_3-ZNO-Al_2O_3-ZNO-Al_2O_3-ZNO-Al_2O_3-ZNO-Al_2O_3-ZNO-Al_2O_3-ZNO-AL_2O_3-ZNO-AL_2O_3-ZNO-AL_2O_3-ZNO-AL_2O_3-ZNO-AL_2O_3-ZNO-AL_2O_3-ZNO-AL_2O_3-ZNO-AL_2O_3-ZNO-AL_2O_3-ZNO-AL_2O_3-ZNO-AL_2O_3-ZNO-AL_2O_3-ZNO-AL_2O_3-ZNO-AL_2O_3-ZNO-AL_2O_3-ZNO-AL_2O_3-ZNO-AL_2O_3-ZNO-AL_2O_3-ZNO-AL_2O_3-ZNO-A$	1.5	402	7.4	55.3	[156]
$Pb_{0.97}La_{0.02}(Zr_{0.33}Sn_{0.55}Ti_{0.12})O_3@SiO_2$	—	238	2.68	_	[157]

Table 3 Energy storage performance of ceramics with core-shell structures



**Fig. 15** (a) SEM images of BNST/MgO ceramics. (b) Dielectric constants, (c) electric potentials, and (d) local electric fields of BNST/MgO ceramics. Reproduced with permission from Ref. [69], © Elsevier Ltd. 2019.

into the BNST ceramics, and more equipotential lines concentrate to a lower value (Figs. 15(c) and 15(d)). Thus the  $E_b$  of the BNST/MgO ceramics changes from 120 to 200 kV/cm via adding 3 wt% MgO insulation phase, and the  $W_{rec}$  of 2.09 J/cm<sup>3</sup> with  $\eta$  of 84% is obtained. Tao *et al.* [70] increased the  $E_b$  of 0.82(0.94BNT-0.06BT)-0.18KNN ceramics from 90 to 140 kV/cm via introducing the ZnO second phase. At the ZnO content of 0.4 wt%, the  $W_{\rm rec}$  of 1.03 J/cm<sup>3</sup> and  $\eta$  of 72.7% are obtained.

### 3.3 Mesoscale modification

The effect of grain size on the energy storage performance is achieved by affecting  $E_b$  [40,150,159].



$$E_{\rm b} \propto ({\rm Grain \ size})^{-a}$$
 (8)

where *a* is in the range of 0.2–0.4 [25,150,160]. In general, the smaller the grain size, the higher the  $E_b$  is [25,150,160–162]. This is mainly due to the formation of the depletion space charge layers at the grain boundary, which efficiently increases the boundary resistivity [25]. As a result, the leakage current decreases in fine-grain ceramics, beneficial to a large  $E_b$  [25]. Up to now, many methods have been successfully utilized in ceramics to reduce grain sizes, such as high-energy ball milling [29,73], novel sintering method [74,163–165], and hydrothermal synthesis [21,22,27,75].

#### 3.3.1 High-energy ball milling

High-energy ball milling is very powerful to reduce the powder size of raw materials through the rotation or vibration, so that the reaction activation energy is dramatically reduced, and the sintering activity is enhanced [166].

Recently, Chen *et al.* [29] successfully reduced the grain size to ~178 nm (Fig. 16(a)) via high-energy ball milling in  $0.6Bi_{0.5}K_{0.5}TiO_3-0.3BaTiO_3-0.1NaNbO_3$  (0.6BKT-0.3BT-0.1NN) ceramics (Fig. 16(b)). Nanoscale grain sizes, dense grain boundaries, ultra-small PNRs, and large  $E_g$  give rise to an ultra-high  $E_b$  of 460 kV/cm and excellent  $W_{rec}$  of ~7.57 J/cm<sup>3</sup>, which is 2.4 times higher than that of previously reported BKT ceramics (Fig. 16(c)) [29]. Moreover, it can be seen that nanoscale modifications and mesoscale modifications are not incompatible. By contrast, they can work together to synergistically improve the energy storage performance.

Compared to that of BiFeO<sub>3</sub>–BaTiO<sub>3</sub>–Bi(Mg<sub>2/3</sub>Nb<sub>1/3</sub>)O<sub>3</sub> (BF–BT–BMN) ceramics prepared via the conventional solid-state (CS) reaction, the grain size prepared via high-energy ball milling reduces from 4.1 to 0.89 µm (Figs. 17(a) and 17(b), respectively) [73]. The TEM reveals layered domains with a width of 80–100 nm in coarse-grained ceramics, while PNRs with a width of ~2 nm are observed in fine-grained ceramics [167]. Therefore, the fine-grained BF–BT–BMN ceramics respond quickly to the external electric field, facilitating the slim and slanted P-E loops (Fig. 17(c)). Most importantly, the  $E_b$  increases from 50 to 110 kV/cm due to the decreased in grain size. Finally, the  $W_{\rm rec}$  of fine-grain ceramics (1.27 J/cm<sup>3</sup>) reaches about 8 times higher than that of coarse-grain ceramics (0.16 J/cm<sup>3</sup>), as shown in Fig. 17(d).

#### 3.3.2 Novel sintering method

Two-step sintering is an effective method to obtain fine-grain ceramics by adjusting the sintering temperature and time. In the one-step sintering process, grain boundary migration and diffusion are always active during both the heating and preservation stage, leading to the grain growth and uneven distribution [74]. During the two-step sintering process, the ceramics are heated to a higher temperature ( $T_1$ ) in the first stage to promote the grain migration and diffusion. In the second stage, the ceramics are rapidly cooled to a lower temperature ( $T_2$ ) and kept for some time. Grain boundary migration and diffusion are thus inhibited, and the grains reach a full density with limited grain boundary diffusion (Fig. 18) [163,168,169].

The  $0.89Bi_{0.5}Na_{0.5}TiO_3-0.06BaTiO_3-0.05K_{0.5}Na_{0.5}NbO_3$ (BNT-BT-KNN) ceramics prepared via one-step sintering have uneven grain distribution and anomalous grains (Fig. 19(a)), while the ceramics with two-step sintering exhibit a much denser crystal morphology with smaller and more homogeneous grains (Fig. 19(b)), leading to the much increased  $E_b$  (Fig. 19(c)) [40,150].



**Fig. 16** (a) SEM image of 0.6BKT-0.3BT-0.1NN ceramics. (b) *P–E* loops and (c) energy storage performance of 0.6BKT-0.3BT-0.1NN ceramics. Reproduced with permission from Ref. [29],  $\bigcirc$  Wiley-VCH GmbH 2021.





**Fig. 17** SEM images of BF–BT–0.06BMN ceramics prepared via (a) planetary ball milling and (b) high-energy ball milling. (c) P-E loops and (d) energy storage performance of BF–BT–0.06BMN ceramics. Reproduced with permission from Ref. [73], © Elsevier Ltd and Techna Group S.r.l. 2021.



**Fig. 18** Different mechanisms of grain growth in one-step sintering process and two-step sintering process. Reproduced with permission from Ref. [74], © Elsevier B.V. 2013.

Wang et al. [164] combined high-energy ball milling with a two-step sintering process and successfully reduced the grain size of 0.925(K<sub>0.5</sub>Na<sub>0.5</sub>)NbO<sub>3</sub>-0.075Bi (Zn<sub>2/3</sub>(Ta<sub>0.5</sub>Nb<sub>0.5</sub>)<sub>1/3</sub>)O<sub>3</sub> (KNN-BZTN) ceramics from 410 to 200 nm (Figs. 20(a) and 20(c), respectively). Accordingly,  $E_{\rm b}$  is increased from 208 to 301 kV/cm. They found that the higher temperature and shorter holding time for the second stage give rise to the smaller grain size and denser microstructures [164]. With a higher temperature, more liquid phase is generated in the ceramics (indicated by the yellow regions in Fig. 20(a1)), while the shorter holding time makes it insufficient for the diffusion, which results in the smaller grain size and more amorphous grain boundaries (Figs. 20(b) and 20(d), respectively) [164]. As a result, the larger resistivity is observed and  $E_{\rm b}$  is increased, doing a great favor to the optimized  $W_{\rm rec}$  of 4.02 J/cm<sup>3</sup> and  $\eta$  of 87.4%.



**Fig. 19** SEM images of BNT–BT–KNN ceramics sintered via (a) one-step sintering and (b) two-step sintering. (c) *P–E* loops of different sintering methods. Reproduced with permission from Ref. [74], © Elsevier B.V. 2013.





**Fig. 20** SEM and high-resolution TEM (HRTEM) images of KNN–BZTN ceramics with different temperature and time: (a, b) 1130 °C, 15 h and (c, d) 1160 °C, 6 h. Note: FWHM means the full width at half maximum. Reproduced with permission from Ref. [164], © The Chinese Ceramic Society 2020.

The two-step sintering is also widely used in other systems. 0.83NaNbO<sub>3</sub>-0.17SrTiO<sub>3</sub> (NN-ST) ceramics prepared via the two-step process show the grain size of ~1.2  $\mu$ m and  $E_b$  of 207 kV/cm [170]. With the decrement in heating/holding temperature and holding time, the grain size gradually decreases from 8.2 to  $1.2 \,\mu m$ , which is conducive to the improvement of  $E_{\rm b}$  (from 128 to 207 kV/cm). Meanwhile, the  $W_{\rm rec}$  and  $\eta$  increase from 0.58 J/cm<sup>3</sup> and 42% to 1.60 J/cm<sup>3</sup> and 50%, respectively. Compared with that of the solid-state sintering, the grain size of BiFeO<sub>3</sub>-SrTiO<sub>3</sub> (BF-ST) ceramics prepared via two-step sintering was only  $3.2 \,\mu\text{m}$ , showing a remarkable decrease by 36% over counterparts prepared by the solid-state sintering [171]. Meanwhile, the  $E_b$  increased from 626 to 750 kV/cm, and the ultra-high  $W_{\rm rec}$  of 8.4 J/cm<sup>3</sup> with  $\eta$  of ~90% was obtained. With the help of two-step sintering, the minimal ceramic grains of ~326 nm was achieved in 0.13Bi(Zn<sub>2/3</sub>(Nb<sub>0.85</sub>Ta<sub>0.15</sub>)<sub>1/3</sub>)O<sub>3</sub> (BZNT)@0.6 wt%SiO<sub>2</sub> MLCC [58]. As a result, the large  $E_{\rm b}$  of 1755 kV/cm was achieved and contributed to the great improvement of  $W_{\rm rec}$  and  $\eta$  by 1261% and 1.9%, respectively.

Besides the two-step sintering, there are some other sintering processes that can also be employed to improve the energy storage performance. For example,

spark plasma sintering (SPS) displays the characteristics of low sintering temperature, rapid heating rate, and short sintering time [172–174]. SPS could effectively suppress the diffusion behavior between the tetragonal  $(Pb_{0.858}Ba_{0.1}La_{0.02}Y_{0.008})(Zr_{0.65}Sn_{0.3}Ti_{0.05})O_3$  (PBLYZST) and the orthorhombic  $(Pb_{0.97}La_{0.02})(Zr_{0.9}Sn_{0.05}Ti_{0.05})O_3$ (PLZST), thus enhancing the FE-AFE switching electric field of PBLYZST-PLZST ceramics to 162 kV/cm. Finally, the  $W_{\rm rec}$  is enhanced to 6.40 J/cm<sup>3</sup>, which is higher than that of CS sintering sample. In addition, hot-press (HP) sintering exposes pressure during the sintering process to promote contact diffusion between particles, which can effectively eliminate pores and refine the grain size [175,176]. Bi<sub>0.5</sub>K<sub>0.5</sub>TiO<sub>3</sub>-Ba(Mg<sub>1/3</sub>Nb<sub>2/3</sub>)O<sub>3</sub> (BKT-BMN) ceramics prepared via the HP process achieve a  $W_{\rm rec}$  of 3.14 J/cm<sup>3</sup>, which is more than two times than that of the sample prepared by the CS sintering [177].

#### 3.3.3 Hydrothermal synthesis

Hydrothermal synthesis is regarded as one of the most suitable methods to obtain fine powders, which is conducive to the preparation of fine-grain ceramics [178,179]. Grain size reduction is an effective and widely used way to improve the  $E_b$  of ceramics without changing the chemical composition, as shown in Table 4.



Composition	Preparation method	Grain size (µm)	$E_{\rm b}$ (kV/cm)	$W_{\rm rec}$ (J/cm <sup>3</sup> )	η (%)	Ref.
AN	Hydrothermal	1.08	273	3.34	54.5	[75]
AN	Hydrothermal	3	216	3.26	53.5	[180]
AN	Hydrothermal	3.4	250	1.85	40	[22]
$Ag_{0.97}Nd_{0.01}NbO_3+MnO_2$	Two-step sintering	1.4	210	3.2	52	[181]
KNN–BZTN	Two-step sintering	0.2	222	4.02	87.4	[164]
NN-ST	Two-step sintering	1.20	207	1.60	50	[170]
$Sr_{0.7}Ba_{0.3}Nb_2O_6$	Two-step sintering	1.34	400	3.2	90	[182]
0.55(0.94BNT-0.06BT)-0.45ST+MnO <sub>2</sub>	Two-step sintering	2.4	280	2.98	73.1	[183]
KNN-H	High-energy ball milling	0.6	740	10.6	90.8	[113]
0.6BKT-0.3BT-0.1NN	High-energy ball milling	0.18	460	7.57	81.4	[116]
$0.9Ba_{0.9}Ca_{0.1}Ti_{0.9}Zr_{0.1}O_3\!\!-\!\!0.1SrNb_2O_6$	High-energy ball milling	0.16	460	2.68	83.4	[184]
						,

Table 4 Energy storage performance of fine-grain ceramics

Wang *et al.* [22] successfully prepared AN fine powders with the particle size of  $\sim$ 480 nm via adjusting the ratio of NH<sub>4</sub>HF<sub>2</sub>, AgNO<sub>3</sub>, and Nb<sub>2</sub>O<sub>5</sub>, from which

AN ceramics with a grain size of  $\sim 3.4 \,\mu\text{m}$  were successfully prepared (Fig. 21(a)). Due to the small grain size, the  $E_b$  of AN is as large as 250 kV/cm



**Fig. 21** (a) SEM images and (b) *P*–*E* loops of AN ceramics prepared via hydrothermal method. (c) Grain sizes and  $E_b$  of AN ceramics prepared by solid-state reaction and hydrothermal method. Breakdown simulations of AN ceramics prepared by (d) solid-state reaction and (e) hydrothermal method. Reproduced with permission from Ref. [22] for (a, b),  $\mathbb{C}$  Elsevier Ltd. 2020; Ref. [75] for (d, e),  $\mathbb{C}$  The Royal Society of Chemistry 2022.

(Fig. 21(b)). The AN ceramics exhibit smaller grain size and larger  $E_{\rm b}$  compared to pure AN ceramics prepared by solid-state reaction (Fig. 21(c)) [34,65, 103,107-109,119,185]. A phase field model, which is used to simulate the spatial distribution of electric potential and electric breakdown paths, also indicates that the smaller grain size of AN ceramics prepared via the hydrothermal method (Figs. 21(d) and 21(e)) and the more breakdown-resistant grain boundaries lead to more energy consumption in the propagation of electrical trees [21,28,75,180]. Huang et al. [75] reported the synthesis of AN ceramics with a grain size of  $\sim 1.08 \,\mu m$  using the hydrothermal synthesized powders. The fine-grain size leads to the increment in  $E_{\rm b}$  up to 273 kV/cm. Finally, the  $W_{\rm rec}$  of 3.34 J/cm<sup>3</sup> and  $\eta$  of 54.5% are achieved in ceramics, which are 1.67 and 1.63 times larger than those prepared via the solid-state reaction, respectively.

#### 3.4 Macroscale modification

#### 3.4.1 Rolling process

High porosity and poor densification of ceramics prepared via the CS reaction are two of the main reasons for the low  $E_b$  [76]. It is simple and effective to prepare energy storage ceramics with high densification and large  $E_b$  via the rolling process. As shown in Fig. 22(a), it involves mixing the ceramic powders with PVA and repeatedly squeezing it through two rotating rolls [48]. In this process, the pores are eliminated by pressure, and the PVA is fully contacted with the powders, giving rise to high-density ceramics [77]. Compared with other preparation processes, the rolling process is characterized by low-cost and simple equipment, which is widely used in the preparation of various ceramics [77,78].

In 2019, Wang *et al.* [48] prepared ( $Pb_{0.98}La_{0.02}$ ) ( $Zr_{0.55}Sn_{0.45}$ )\_{0.995}O<sub>3</sub> (PLZS) ceramics with high relative

densities and  $E_b$  via the rolling process. The ceramics display smaller grain sizes, fewer pores, and higher relative densities (> 97%), which are expected to improve the  $E_b$  (Figs. 22(b) and 22(c)). Ultimately, the prepared PLZS ceramics exhibit an ultra-high  $W_{\rm rec}$  of 10.4 J/cm<sup>3</sup> with  $\eta$  of 87% at 410 kV/cm, which is the highest  $W_{\rm rec}$  value among the bulk materials at that time.

The rolling process is also applied to BT-based ceramics [186]. Compared with the CS reaction, the rolling process can reduce the grain size of  $(Ba_{0.65}Sr_{0.245}Bi_{0.07})_{0.99}Nd_{0.01}TiO_3$  (BT–SBT–Nd) ceramics and make a uniform grain distribution [77]. The  $E_b$  of the ceramics increases from 275.5 to 468.9 kV/cm due to the improved relative densities, and the *P*–*E* curves exhibit a larger polarization of ~35  $\mu$ C/cm<sup>2</sup>. Finally, the  $W_{rec}$  of 4.2 J/cm<sup>3</sup> is obtained, which is ~2.1 times larger than that obtained via the CS reaction.

# 3.4.2 Tape-casting process

The tape-casting process involves mixing ceramic powders with solvents, dispersants, binders, and plasticizers to form a homogeneous suspension, which is then prepared into a thin, continuous ceramic ribbon using a scraper [187]. The ribbon has high relative densities and can be thinned to less than 50 µm in thickness [23,187]. Many layers of ceramic ribbons with electrodes coated via screen printing are stacked in a certain way and hot pressed. Finally, the MLCCs are obtained after burning out the binder by sintering, as shown in Fig. 23 [187]. The tape-casting process displays the following two advantages: (1) Compared to CS reaction, it facilitates ceramic layers with lower porosity and finer grain size, which lead to higher  $E_{\rm b}$ [5]. (2) For the same capacitor volume, a higher  $E_b$  is expected in the MLCCs compared to that of the bulk ceramics, as the  $E_{\rm b}$  exponentially increases with the decreased layer thickness [25,188].



**Fig. 22** (a) Schematic diagram of rolling process. SEM images of ceramics prepared via (b) rolling and (c) traditional method. Reproduced with permission from Ref. [48], © WILEY-VCH Verlag GmbH & Co. KGaA, Weinheim 2019.





**Fig. 23** Schematic diagram of MLCC preparation process. Reproduced with permission from Ref. [187], © IEEE 2010.

In 2018, Li *et al.* [5] prepared the 0.55(Na<sub>0.5</sub>Bi<sub>0.5</sub>) TiO<sub>3</sub>–0.45(Sr<sub>0.7</sub>Bi<sub>0.2</sub>)TiO<sub>3</sub> (0.55NBT–0.45SBT) MLCCs with an ultra-high energy density and energy efficiency via the tape-casting process. Compared with that of the bulk ceramics, the thickness of single layer is reduced from ~200 to ~20  $\mu$ m. The  $E_b$  is thus increased from 200 to 720 kV/cm (Figs. 24(a) and 24(b)). The decreased thickness reduces the probability of defects. With the substantial increment in  $E_b$ , the  $W_{rec}$  also elevates from 2.5 to 9.5 J/cm<sup>3</sup> and still maintains an ultra-high  $\eta$  of 90%.

Later, Li et al. [57] combined the tape-casting process with texture engineering to construct <111>-textured NBT-0.35SBT MLCCs. Ceramic capacitors will generate strain and elastic energy under an external electric field, which may result in the electromechanical breakdown [189]. The electrostriction of perovskite structures generally exhibits obvious anisotropy. In particular, the electrostriction strain coefficient in the <100> directions is about 4–5 times larger than that in the <111> directions [190]. Under an electric field of 50 MV/m, the strain of <111>-textured ceramics is only 0.19%, which is much reduced compared with that of nontextured ceramics (0.55%) (Fig. 24(c)). Benefiting from the much reduced strain, the  $E_b$  of <111>-textured ceramics achieves 103 MV/m, which is 61% higher than that of nontextured ceramics (~64 MV/m) (Fig. 24(d)). The multi-scale synergic optimization of elemental modification, texture engineering, and tape-casting process plays a very important role in optimizing the energy storage properties. The  $W_{\rm rec}$  of ~21.5 J/cm<sup>3</sup> with  $\eta$  of ~80% is realized in <111>-textured ceramics, which is 1.5 times larger than that of the nontextured counterparts (Figs. 24(e) and 24(f)).

Zhu *et al.* [23] reported the ANT+0.25 wt%  $MnO_2$  MLCCs with the ultra-high  $E_b$  by adjusting the thickness of active and inactive layers. Ultimately, due



**Fig. 24** *P–E* loops of (a) 0.55NBT–0.45SBT bulk ceramics and (b) 0.55NBT–0.45SBT MLCCs. (c) Strain vs. electric field curves and (d)  $E_b$  of <111>-textured and nontextured MLCCs. Energy storage performance of (e) nontextured and (f) <111>-textured multilayer ceramics. Reproduced with permission from Ref. [5] for (a, b), © WILEY-VCH Verlag GmbH & Co. KGaA, Weinheim 2018; Ref. [57] for (c–f), © The Author(s), under exclusive licence to Springer Nature Limited 2020.

to the small grain size, low leakage current, and thin thickness, the  $E_b$  of 1020 kV/cm is achieved, 343% larger than that of bulk ceramics [23,34]. The energy density is accordingly increased from 4.2 to 7.9 J/cm<sup>3</sup>.

The decreased dielectric layer thickness induced by the tape-casting process is the main reason for the enhancement of  $E_{\rm b}$ . MLCCs prepared via the tapecasting process are one of the most widely used method for commercial ceramic capacitors [58,191,192]. Zhao et al. [193] prepared an RFE multilayer energy storage ceramic capacitor (MLESCC) of 0.87BT-0.13BZNT with a dielectric layer thickness of 5  $\mu$ m. The  $E_b$  is increased to 1060 kV/cm, and Wrec is increased to 10.12 J/cm<sup>3</sup>. Later, they combined tape-casting process with a core-shell structure to prepare a BT-BZNT@SiO2 MLCC with  $E_b$  up to 175.5 MV/m and the giant  $W_{rec}$  of 18.24 J/cm<sup>3</sup> with ultra-high  $\eta$  of 94.5% [58]. With the help of decreased dielectric layer thickness,  $E_{\rm b}$  of  $(Pb_{0.875}La_{0.05}Sr_{0.05})$   $(Zr_{0.695}Ti_{0.005}Sn_{0.3})O_3$  (PLSZTS) is also increased from 555 kV/cm (bulk) to 850 kV/cm (MLCC). The ultrahigh  $W_{\rm rec}$  of 19.2 J/cm<sup>3</sup> and  $\eta$  of 96.4% are therefore obtained [194].

#### 3. 5 Multi-scale synergic optimization

In the previous sections, it can be seen that the modification strategies at various scales play their distinct roles in enhancing the energy storage performance. And it is rational to anticipate that the synergetic modifications at multi-scales can boom the energy storage potential of dielectrics better. Take the multi-scale modifications of BT–BZNT MLCC as an example [195]. At the nanoscale, RFE BT ceramics can be obtained by introducing BZNT; at the mesoscale, the reduced grain sizes are achieved via two-step sintering and at the macroscale, and the tape-casting process can

reduce the thickness of the single layer of dielectrics. With the combination of the above effects, the  $E_{\rm b}$  up to 750 kV/cm and the high  $W_{\rm rec}$  of 8.13 J/cm<sup>3</sup> with ultra-high  $\eta$  of 95% were finally achieved. Wang *et al.* [188] also successfully obtained high-performance BT-BZNT@SiO<sub>2</sub> MLCC via combining the above effects and the core-shell structure, in which giant  $W_{\rm rec}$ of 18.24 J/cm<sup>3</sup> and  $\eta$  of 94.5% were obtained under a large electric field of 1755 kV/cm. Wang et al. [196] used Al<sub>2</sub>O<sub>3</sub> and SiO<sub>2</sub> to wrap BT powders to build the core-shell structure. Meanwhile, the tape-casting process was utilized to reduce the single layer thickness of the ceramic from 63 to 12  $\mu$ m. As a result, the  $E_{\rm b}$  of the BT@(Al<sub>2</sub>O<sub>3</sub>+SiO<sub>2</sub>) MLCC was increased from 184 to 665 kV/cm, giving rise to the > 250% enhancement in  $W_{\rm rec}$  (i.e., from 1.14 to 4.06 J/cm<sup>3</sup>).

In addition, there are many other combinations of multi-scale optimization strategies, including but not limited to the phase engineering combined with highenergy ball milling [33], the synergic modulations involving the hydrothermal synthesis, phase engineering, and constructing core–shell structure [27], and the comprehensive optimization of domain engineering combined with two-step sintering [164].

## 4 Summary and perspectives

The modification methods at different scales have their own characteristics. Figure 25 summarizes the typical modification methods for ceramics reported so far [23,28,47,48,52,58,62,64,71,73,75,95,103,116,117,119, 130,141,142,156,164,172,181,193,194,197–212]. With the continuous development of electronic information technology, the demand for dielectric capacitors in the



Fig. 25  $W_{\rm rec}$  of energy storage ceramics after modification by different methods.



field of high-power/pulsed devices is increasing. Ideal energy storage capacitors need to possess high polarization, low loss, and large  $E_{\rm b}$ . This review summarizes the multi-scale modification strategies of ceramics from the nanoscale, microscale, mesoscale, and macroscale and lists some common features.

1) At the nanoscale: Modulating the phase and domain structures via doping or forming solid solutions is a simple and effective method. Ceramics normally have a variety of complex phase structures, which accordingly give rise to different performance. The energy storage property is often optimized by stable AFE phase regions (the AFE<sub>0</sub> phase region in PLZT ceramics), relaxor phase boundaries (the M<sub>2</sub>–M<sub>3</sub> phase boundary in AN ceramics), etc. Domain engineering is usually achieved via the nanoscale PNRs. These nanodomains are sensitive to the external electric field, which can reduce hysteresis and improve the energy efficiency. Moreover, the energy storage performance can be improved by special elements that can enhance the  $E_g$  (CH) or polarization (Bi<sup>3+</sup> and W<sup>6+</sup>).

2) At the microscale: The "core–shell" structure was constructed via depositing a coating layer with low dielectric constants (such as SiO<sub>2</sub> and ST) on the ceramic grains, which can improve the  $E_b$ , maintain the high polarization, and finally reach excellent energy storage properties.

3) At the mesoscale: There is a strong link between the ceramic grain size and  $E_b$ , that is,  $E_b$  increases exponentially with the decreased grain size. Therefore, the preparation of fine-grain ceramics via high-energy ball milling, two-step sintering, or hydrothermal synthesis can significantly optimize the  $E_b$  and improve the energy density. Constructing 0–3 type composites through interface design can also enhance the energy storage performance.

4) At the macroscale: The rolling process can greatly improve the relative density of the ceramics, and the tape-casting process can reduce the monolayer thickness down to  $< 50 \mu$ m, which would greatly facilitate the  $E_{\rm b}$ . It also enables the stacking of multilayer ceramics to achieve the integration of ceramic capacitor devices and enhances the practical application capability.

In addition, ceramic films serving as a special kind of high energy storage material show great potential for high  $E_{\rm b}$  and  $W_{\rm rec}$  due to the reduced thickness (< 1 µm) and the formation of polymorphic nanodomains. Up to now, extensive efforts have been paid on dielectric ceramic films, and the  $W_{\rm rec}$  of 50–300 J/cm<sup>3</sup>,  $\eta$  of 60%–90%,  $E_{\rm b}$  of 1–6 MV/cm, and thermal stability over the range of –50–200 °C have been successfully achieved. And better comprehensive energy storage performance is highly anticipated with the development of large-area epitaxial film deposition. Moreover, the thick films and multilayered films can also be explored to further enhance the energy density. Ceramic films are becoming a rising star in the dielectric energy storage ceramics.

With the great effects of many research groups for decades, ceramic capacitors have achieved significantly excellent energy storage properties, but there are still many challenges. For example, the failure mechanism under long-term cyclic operation is still not clear. Especially, the generated thermal energy and mechanical energy during the charge/discharge cycling will seriously affect the performance and service life of capacitors. Therefore, it is important and urgent to study the failure mechanism of dielectric capacitors under multi-field including but not limited to force, electric, and thermal coupling conditions in long-term cyclic operation.

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#### **Declaration of competing interest**

The authors have no competing interests to declare that are relevant to the content of this article.

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